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AIR FORCE CAMBRIDGE RESEARCH LABORATORIES

L. G. HANSCOM FIELD, BEDFORD, MASSACHUSETTS

UV, Visible, and IR Attenuation for Altitudes to 50 km, 1968

L. ELTERMAN

OFFICE OF AEROSPACE RESEARCH United States Air Force





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OPTICAL PHYSICS LABORATORY

PROJECT 7470

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Abstract

An atmospheric attenuation model for the ultraviolet, visible, and infrared was developed in 1964, based on scattering (molecules and aerosols) and ozone absorption. Since then more measurements have been made and our knowledge of aerosol attenuation has widened. These circumstances result in attenuation model changes which are relatively unimportant for most exploratory calculations. They can be significant, however, for long slant-path high-altitude applications entailing large zenith angles, factors which characterize, for example, the measurement geometries of rockets and satellites. Accordingly, a revision of the 1964 Attenuation Model is warranted.

In this paper the optical parameters are computed spectrally and with altitude as follows: (1) pure air attenuation parameters are determined by utilizing Rayleigh scattering cross sections with molecular number densities from the standard atmosphere; (2) ozone absorption parameters are derived based on Vigroux's coefficients applied to a representative atmospheric ozone distribution; (3) seven sets of aerosol measurements are compared and a profile of aerosol attenuation coefficients vs altitude is developed. Attenuation coefficients and optical thickness due to molecular, aerosol, and ozone attenuation are computed and tabulated individually so that the influence of each can be compared. The newly derived tabulations permit various exploratory calculations, including horizontal, vertical, and slant-path transmission at kilometer intervals to an altitude of 50 km, individually for each attenuating component or for overall atmospheric extinction (molecular + ozone + aerosol).

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Parameters at 0.27 to 4.00 (Tables 4.1 to 4.22)

Symbols

```
Vigroux ozone absorption coefficient (cm<sup>-1</sup>)
\mathbf{D_3}
             Ozone concentration (cm/km)
             Horizontal path length (km)
H
             Aerosol scale height (km)
             Altitude (km)
ĸ
             Mie scattering efficiency
             Aerosol index of refraction
m
             Index of refraction at sea level, air at 1013 mb and 15°C
m_
N<sub>3</sub>
             Ozone number density (cin<sup>-3</sup>)
             Aerosol number density (cm<sup>-3</sup>)
             Molecular number density (cm<sup>-3</sup>)
             Molecular number density at sea level (cm<sup>-3</sup>)
             Particle radius (microns)
             Turbidity (\beta_p/\beta_r)
Temperature °K
T<sub>h</sub>
             Horizontal transmission
             Transmission between sea level and altitude h
T<sub>h-∞</sub>
T<sub>Δh</sub>
             Transmission between h and space
             Transmission between two altitudes above sea level
             Atmospheric ozone absorption coefficient (km<sup>-1</sup>)
β<sub>3</sub>
             Aerosol attenuation coefficient (km<sup>-1</sup>)
            Mean of 79 profiles for \lambda_1 = 0.55 microns (km<sup>-1</sup>)
```

β_r	Rayleigh attenuation coefficient (km ⁻¹)
β _{ext}	Extinction coefficient (km ⁻¹)
δ	Depolarization factor
в	Zenith angle
λ	Wavelength (microns or cm)
λ,	Wavelength 0.55 microns
o'r	Rayleigh scattering cross section (cm ²)
r_3	Ozone optical thickness from sea level to altitude h (0-h)
7 1 3	Ozone optical thickness from altitude h to space (h)
τ p	Aerosol optical thickness from sea level to altitude h, (0-h)
71	Aerosol optical thickness from altitude h to space, (h-∞)
τ τ	Rayleigh optical thickness from sea level to altitude h, (0-h)
$ au_{\mathbf{r}}^{\mathbf{i}}$	Rayleigh optical thickness from altitude h to space, (h-∞)
r _{ext}	Extinction optical thickness (molecular + ozone + aerosol) from sea level to altitude h, (0-h)
ri ext	Extinction optical thickness (molecular + ozone + aerosol) from altitude h to infinity, (h)
Ψ	Aerosol size distribution function

UV, Visible, and IR Attenuation for Altitudes to 50 km, 1968

1. INTRODUCTION

In 1964, an atmospheric attenuation model was published (Elterman, 1964) which has been useful for a variety of exploratory calculations. Now a revision is warranted for reasons given in the abstract and Section 4 of this report. In this revision most of the earlier material is presented in summary form. The section on attenuation by Rayleigh scattering, however, is retained because the content leading to the derivation of the Rayleigh parameters is useful. In one instance, due to existing interest, the material is expanded, i.e., the tabulations which comprise the attenuation model now include aerosol and ozone optical thickness so that a comparison can be made of the relative importance of each attenuating component for vertical and slant paths.

The shortest wavelength considered is 0.27 microns. The use of shorter wavelengths would require a treatment of $\rm O_2$ absorption. Also, attenuation is sufficiently severe so that interest in the shorter wavelength region for purposes of ultraviolet transmission below 50 km probably is limited. The longest wavelength used is 4.0 microns. Calculations for longer wavelengths are complicated by the presence of absorption bands of $\rm H_2O$, $\rm CO_2$, and their wings. In between, a total of 22 wavelengths is chosen (Table 1) within the atmospheric windows and for the ultraviolet region where ozone absorption is important.

⁽Received for publication 25 March 1968)

Conceptually, the attenuation model starts with molecular, densities from the latest published U.S. Standard Atmosphere (1962) followed by the addition of ozone and aerosol components. The meteorological range (M.R.) at sea level corresponds to about 25 km at 0.55 μ wavelength. This choice serves a useful function because it permits including some important measurements conducted at $\lambda \approx 0.55 \mu$. In addition, this wavelength customarily represents the phototopic region.

Table 1. Model Parameters as a Function of Wavelength

			والمراكب والمراكب والمراكب
λ (microns)	ms	σ _r (cm²)	A _v (cm ⁻¹)
0.27	1.00029668	8.960×10^{-26}	2.10 × 10 ²
0.28	1.00029475	7.646×10^{-26}	1.06×10^{2}
0.30	1.00029156	5.677×10^{-26}	1.01 × 10 ¹
0.32	1.00028902	4.310×10^{-26}	8.98×10^{-1}
0.34	1.00028699	3.334×10^{-26}	6.40×10^{-2}
0.36	1.00028531	2.622×10^{-26}	1.80 × 10 ⁻³
0.38	1.00028392	2.091×10^{-26}	0
0.40	1.00028275	1.689×10^{-26}	0
0.45	1.00028052	1.038 × 10 ⁻²⁶	3.50×10^{-3}
0.50	1.00027896	6.735×10^{-27}	3.45×10^{-2}
0.55	1.00027782	4.563×10^{-27}	9.20×10^{-2}
0.60	1.00027697	3.202×10^{-27}	1.32×10^{-1}
0.65	1.00027630	2.314×10^{-27}	6.20×10^{-2}
0.70	1.00027578	1.714×10^{-27}	2.30×10^{-2}
0.80	1.00027503	9.990×10^{-28}	1.00 × 10 ⁻²
0.90	1.00027451	6.213×10^{-28}	0
1.06	1.00027397	3.216 × 10 ⁻²⁸	0
1.26	1.00027357	1.606 × 10 ⁻²⁸	0
1.67	1.00027315	5.189 × 10 ⁻²⁹	0
2.17	1.00027292	1.817×10 ⁻²⁹	0
3,50	1.00027272	2.681 × 10 ⁻³⁰	0
4.00	1.00027269	1.571 × 10 ⁻³⁰	0

λ - Wavelength

m_g - Index of refraction (1013 mb, 15°C)

 a_{r} - Rayleigh scattering cross section

Av - Absorption coefficient after Vigroux for pure O3, smoothed values (1013 mb, 18°C)

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2. RAYLEIGH PARAMETERS

A fundamental requirement for generating an accurate series of Rayleigh parameters is an exact determination of the index of refraction for the wavelengths of interest. With this known, the Rayleigh cross sections can be computed. This in turn permits computation of the Rayleigh attenuation coefficient and its variation with altitude as well as corresponding optical thickness values.

The index of refraction for a standard atmosphere (1013 mb, 15°C) specifically for the desired wavelengths used is determined by Edlen's (1953) expression

$$(m_g - 1)10^{-8} = 6432.8 + \frac{2949810}{146 - (\lambda^{-2})} + \frac{25540}{41 - (\lambda^{-2})}$$
, (1)

where mg = refractive index ,

 λ = wavelength (microns).

Penndorf's (1957) computations using Eq. (1) demonstrate that the effect of water vapor can be neglected and the derived $m_{\rm g}$ values have negligible error for the spectral range from 0.2 to 20.0 microns.

The Rayleigh cross section is expressed by

$$\sigma_{r}(\lambda) = \frac{8\pi^{3}(m_{g}^{2}-1)^{2}}{3\lambda^{4}N_{g}^{2}} \cdot \frac{6+3\delta}{6-7\delta}$$
 (2)

where

 σ_{n} = the Rayleigh scattering cross section (cm²),

 λ = the wavelength (cm),

n_ = the index of refraction of air at 15°C and 1013 mb pressure,

 N_s = the molecular number density at sea level for a standard atmosphere (cm $^{-3}$),

 δ = the depolarization factor.

The term $(6+3\delta)/(6-7\delta)$ accounts for the degree of depolarization attributable to the anisotropy of the atmospheric molecule. The depolarization factor has been determined by calculation and by laboratory measurement. The latest work of Gucker and Basu (1953) yields $\delta \approx 0.035$. The wavelengths of interest with the indices of refraction and Rayleigh cross sections [computed from Eqs. (1) and (2)] are listed in Table 1, and plotted in Figures 1 and 2.

Using the scattering cross sections, the Rayleigh coefficients are obtained with

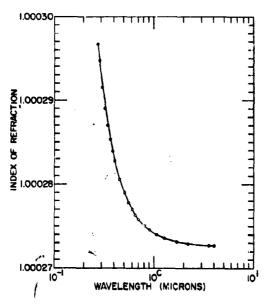


Figure 1. Index of Refraction for 1013 mb and 15°C (Table 1), 0000 Represent Attenuation Model Wavelengths

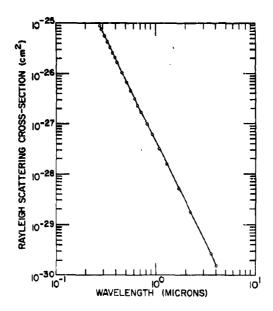


Figure 2. Rayleigh Cross Section vs Wavelength (Table 1), 0000 Represent Attenuation Model Wavelengths

$$\beta_{n}(h,\lambda) = \sigma_{n}(\lambda) \cdot N_{n}(h) \cdot (10^{9} \text{ cm/km}) , \qquad (3)$$

where

 β_r = the Rayleigh attenuation coefficient (km⁻¹),

 σ_r^1 = the Rayleigh scattering cross section (cm²),

 N_{n} = the molecular number density (cm⁻³).

The values of $N_r(h)$ needed for Eq. (3) were obtained from the U.S. Standard Atmosphere and are listed in Table 2. This expression is used to compute an array of Rayleigh attenuation coefficients as a function of altitude for each wavelength.

With the Rayleigh attenuation coefficients determined, the optical thicknesses from sea level to some altitude h are computed by

$$\tau_{\mathbf{r}}(\mathbf{h},\lambda) = \sum_{0}^{h} \bar{\beta}_{\mathbf{r}}(\mathbf{h},\lambda) \Delta \mathbf{h} , \qquad (4)$$

where

 $\tau_{\rm r}$ = Rayleigh optical thickness (0 - h),

 $\tilde{\beta}_r^*$ = mean of the Rayleigh attenuation coefficients (km⁻¹) for each altitude increment,

 Δ h = altitude increment chosen as one km for these calculations.

The Rayleigh optical thickness for altitude h to space is obtained by the relationship

$$\tau_{\mathbf{r}}^{\dagger}(\mathbf{h}, \lambda) = \tau_{\mathbf{r}}^{\dagger}(\infty, \lambda) - \tau_{\mathbf{r}}^{\dagger}(\mathbf{h}, \lambda)$$
, (5)

where

 $\tau_r^t(h)$ = Rayleigh optical thickness $(h \sim \infty)$,

 $\tau_r(\infty) = \text{Rayleigh optical thickness } (0 - \infty)$.

The term $\tau_r(\infty)$ was obtained by using Eq. (4) with the limits set between 0 and 80 km. Above 80 km, Stergis' (1966) calculations, based on N₂, O₂, and O as the principal atmospheric constituents, yield

$$\int_{80}^{\infty} \beta_{\mathbf{r}}(h,\lambda) dh = \begin{bmatrix} 3.6 \times 10^{-6} , \lambda = 0.4 \,\mu \\ 6.7 \times 10^{-7} , \lambda = 0.6 \,\mu \\ 2.1 \times 10^{-7} , \lambda = 0.8 \,\mu \end{bmatrix}.$$

These values approximate a constant 10^{-5} , that of the Rayleigh optical thickness for unity air mass. For our purposes then the integral can be neglected because the constant is small and applies to all wavelenging of interest.

Table 2. Model Parameters as a Function of Altitude

F=====		
h (km)	N _r (cm ⁻³)	D ₃ (cm/km)
0 1 2 3 4 5 6	2.547 × 10 ¹⁹ 2.311 2.093 1.891 1.704 1.531 1.373	3.56 × 10 ⁻³ 3.26 / (2.93 2.50 2.26 2.21 2.16
7	1.227	2.23
8	1.093	2.28
9	9.712×10 ¹⁸	2.81
10	8.598	3.50
11	7.585	4.60
12	6.486	6.21
13	5.543	8.45
14	4.738	9.57
15	4.049	9.94
16	3.461	1.03 × 10 ⁻²
17	2.959	1.11
18	2.529	1.22
19	2.162	1.42
20	1.849	1.64
21	1.574	1.84
22 23 24 25 26 27 28	1.341 1.144 9.760 × 10 ¹⁷ 8.335 7.123 6.092 5.214	1.97 1.98 1.93 1.80 1.63 1.41
29	4.466	1.07
30	3.828	9.03 × 10 ⁻³
31	3.283	7.93
32	2.818	6.82
33	2.406	5.82
34	2.056	4.85
35	1.760	4.31
36	1.509	3.61
37	1.296	3.02
38	1.116.	2.53
39	9.620×10 ¹⁶	2.17
40	8.308	1.86
41	7.187	1.52
42	6.227	1.19
43	5.404	9.30 × 10 ⁻⁴
44	4.697	7.44
45	4.088	5.76
46	3.564	4.46
47	3.112	3.53
48	2.738	2.79
49	2.418	2.23
50	2.135	1.86

h-Altitude; $N_r-Molecular$ number density; $D_3-Ozone$ equivalent thickness

3. ABSORPTION PARAMETERS FOR ATMOSPHERIC OZONE

This section is a summary of the material used in the 1964 Attenuation Model. The parameter for determining O_3 absorption as a function of altitude is the atmospheric ozone absorption coefficient expressed by:

$$\beta_3(h,\lambda) = A_v(\lambda) D_3(h)$$
, (6)

 β_3 = atmospheric ozone absorption coefficient (km⁻¹),

 $A_v =$ the pure ozone absorption coefficient (cm⁻¹) after Vigroux,

D₃ = the ozone equivalent thickness (cm/km).

Thus, the Vigroux coefficients (1953) listed in Table 1 in conjunction with the ozone concentrations, Table 2 and Figure 3, permit the computation of an array of atmospheric ozone absorption coefficients to 50 km for each of the desired wavelengths.

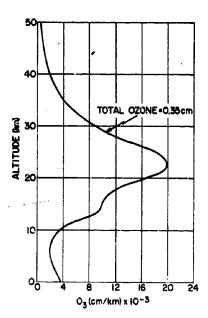


Figure 3. Representative Atmospheric Ozone Concentration Profile (Table 2). Values for: 0 to 30 km, based on Handbook of Geophysics and Space Environment (1965) 30 to 40 km, interpolated 40 to 50 km, based on London, Ooyama, and Prabhakara (1962)

The ozone optical thickness from sea level to altitude h, $\tau_3(h,\lambda)$, and the ozone optical thickness from some altitude h to space, $\tau_3'(h,\lambda)$, are included in the model tabulations. The expressions for deriving these parameters have the same form as Eqs. (4) and (5).

4. AEROSOL ATTENUATION

Of the various methods used to investigate aerosol attenuation, for the present we will consider optical techniques only because they are suited to this type of study. In this country, Newkirk and Eddy (1964) used solar aureole photometry; Penndorf (1954) analyzed solar radiation measurements from aircraft altitudes; Elterman's results (1966a,b), with searchlight probing, comprise a substantial number of profiles acquired in New Mexico for altitudes to about 34 km. In Australia, Crosby and Koerber (1962) used a balloon-borne integrating nephelometer. In the U.S.S.R., Kondratiev, et al. (1967), conducted balloon solar transmission measurements; Fecktistov (1965) analyzed photographs of the earth's horizon from the spacecraft Voschod: Rozenberg, et al. (1960) (1966), acquired their results with searchlight probing. The various results, as shown in Figure 4, were made comparable at $\lambda_{\rm s}=0.55\mu$ by using the empirical relationship that the aerosol attenuation coefficient is inversely proportional to wavelength. For reasons of clarity, a substantial body of results was not included in Figure 4, as for example the twikight measurements by Rozenberg (1965), Volz and Goody (1962), the searchlight measurements by Spankuch (1967), analysis of twilight aureole photographs from the spacecraft Vostok-6 by Driving (1966), the aircraft measurements of sky brightness by Sandomirski, Al'tovskaja and Trifonova (1964), and aircraft nephelometry by Waldram (1945). Also, interesting results in the form of relative values have been obtained with optical techniques: the twilight measurements by Bigg (1964), the laser beam backscatter by Collis and Ligda (1966), by Clemeshaw, Kent, and Wright (1967), and by Grams and Fiocco (1967).

A consideration of all results shows, as does Figure 4, that the aerosol attenuation coefficient is a strongly fluctuating parameter and that average values based on an adequate number of measurements are necessary in order to establish a representative profile. The recent searchlight probing measurements (Elterman, 1966a and 1966b) appear representative based on several considerations. First, each profile was acquired by continuous measurement through both troposphere and stratosphere and with an altitude resolution approximating one km. In addition, a total of 119 profiles comprising absolute values of aerosol attenuation coefficients were determined for various times throughout the year. This represents a substantially larger sample than previously published. Further, such a quantity of

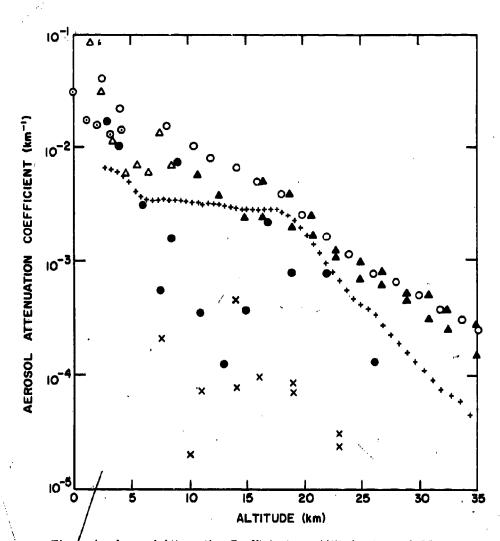


Figure 4. Aerosol Attenuation Coefficients vs Altitude at $\lambda_1=0.55\mu$. Comparison of results: $\times \times \times \times$ solar aureole, 2 balloon flights, Newkirk and Eddy (1964); $\Delta \Delta \Delta \Delta \Delta$ solar radiation measured from aircraft, mean of 8 flights, Penndorf (1954); searchlight probing, mean of 105 profiles, Elterman (1966a) and (1966b);

balloon integrating nephelometer, mean of 14 flights, Crosby and Koerber (1962);

solar radiation measured from balloons, mean of 3 flights, Kondratiev et al. (1967); spacecraft horizon photography, analysis of 4 frames, Rozenberg (1966), Feoktistov (1965); searchlight probing, mean for 5 nights, Rozenberg (1966)

results readily permits statistical treatment. Finally, we note that the mean of the 119 profiles falls reasonably well within the values determined by other researchers, a circumstance which tends to provide a measure of comfort.

In considering the suitability of the 119 profiles, extensive averaging is required and this tends to wash out features easily noted in the individual profile. We present, therefore, in Figure 5 a single profile, chosen because its properties are readily evident and also because it is similar to the overall average. The features can be made to emerge more prominently if the aerosol coefficients are used to compute a turbidity profile, $t_p(h,\lambda_1) = \beta_p(h,\lambda_1)/\beta_r(h,\lambda_1)$, where β_p and β_r are the aerosol and Rayleigh coefficients respectively and $\lambda_1 = 0.55\mu$ (Figure 6).

Since volcanic dust in the atmosphere can have a residence time of several years, the effects of the Mt. Agung eruption (March 1963) must be considered. The direct measurements of Junge, Chagnon, and Manson (1961), Friend (1965), Mossop (1964), and Rosen (1968), collectively considered, before and after this event, show evidence of change in the stratospheric aerosol content. The observations of the twilight sky by Volz (1965) and Meinel and Meinel (1964) also show augmentation of stratospheric particulates. Since the searchlight probing measurements yielded absolute values of aerosol attenuation coefficients, the most suitable parameter to use for examining this feature quantitatively is the stratospheric aerosol optical thickness for the altitude region between the tropopause and 25 km. The reason for choosing the latter altitude limit will be discussed later. Accordingly, all profiles were placed in time-sequential groups determined by the similarity of the stratospheric dust feature. Then the optical thickness was computed by

$$\vec{\tau} = \frac{1}{n} \sum_{i=1}^{n} \sum_{h_1}^{h_2} \bar{\beta}^{i}(h) \Delta h$$
 , (7)

where n is the number of profiles in the group, h_1 is the altitude of the tropopause, h_2 the 25 km altitude, $\overline{\beta}$, the mean aerosol attenuation coefficient (within each profile) for the altitude interval, and Δh the altitude intervals used for computing the profiles. The results of this computation are presented in Table 3. The tabulation demonstrates a relatively high level of stratospheric dust for the December 1963 to March 1964 period. Beginning with April 1964, dust abatement and a generally stabilized level are in evidence. The mean optical thickness of Group (B+C+D) is 26 percent less than that of Group A. Since Group A entails a period of abnormally high aerosol content, its profiles are not representative. These results are in satisfactory agreement with the findings from the direct measurements of the authors mentioned.

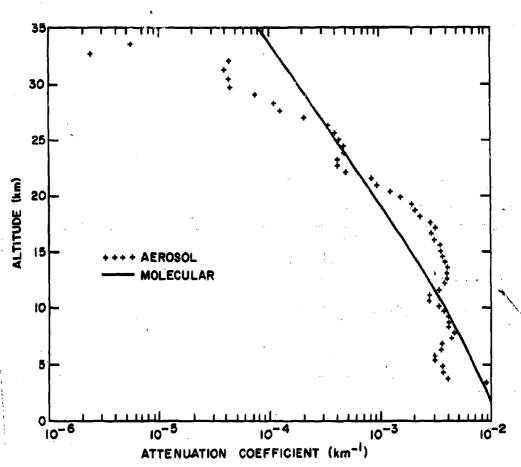


Figure 5. Single Profile $\beta_p(h,\lambda_1)$ for 11 April 1964 at 02:00 MST, Similar to Mean of 79 Profiles, λ_1 = 0.55 μ . Surface to 5 km - convective region; 5 to 11.7 km - troposphere dust layer; 11.7 to 23.8 km - stratosphere dust layer; 25.6 km - upper altitude maximum + + + + aerosol (measurements) molecular (computed)

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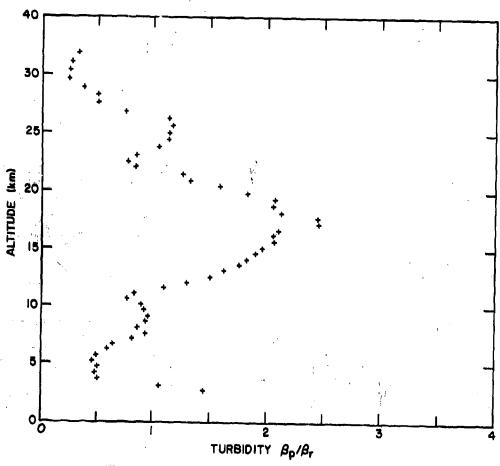


Figure 6. Single Turbidity Profile $\beta_p(h, \lambda_1)/\beta_r(h, \lambda_1)$ for 11 April at 0200 MST. +++++ Measurements (See caption pertaining to Figure 5)

Table 3. Aerosol Optical Thickness as a Measure of Volcanic Dust, λ_1 = 0.55 μ

Group	Period (Inclusive)	Number of Profiles	Mean Optical Thickness (approx. 12-25 km)
A	Dec 1963 - Mar 1964	40	3.1 × 10-2
. B	Apr 1964 - Sep 1964	50	2.2
C	Oct 1964 - Nov 1964	10	2.7
D	Dec 1964 - Apr 1965	19	2.4
B+C+D	Apr 1964 - Apr 1965	79	2.3

The considerations discussed above justify the selection of the Group (B+C+D) profiles as a basis for developing representative aerosol attenuation parameters. It will be convenient to designate the 7s profile average for $\lambda_1 = 0.55 \mu$ as $\bar{\beta}_p(h,\lambda_1)$ (Figure 7). This profile can be extended to encompass a larger altitude range by using the scale height relationship,

$$\bar{\beta}_{p}(h_{2}, \lambda_{1}) = \bar{\beta}_{p}(h_{1}, \lambda_{1}) \exp \left[-\frac{(h_{2} - h_{1})}{H_{p}} \right]$$
 (8)

Penndorf's study (1954) shows that for the lowest 5 km, the aerosol coefficients fall off exponentially with a scale height $0.97 < H_p < 1.4$ km. We resort to the use of his mean value, $H_p = 1.2$ km, to extend the $\beta_p(n, \lambda_1)$ profile from 3.7 km to sea level. This results in aerosol coefficients which are identical to those of the 1964 Attenuation Model for altitudes 0 to 3 km (Table 4.11).

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Above the convective region, up to the tropopause the aerosol coefficients show a moderate gradient which is in close agreement with Penndorf's analysis (1954) of the vertical distribution of aerosols in the troposphere. Also, this section of the profile is based on high signal to noise measurements and extensive averaging, factors which contribute to its reliability. Additionally, this altitude region, being above the convective layer, is characterized by aerosol conditions which tend to be independent of surface terrain. These considerations suggest that the shape and values of the $\hat{\beta}_{\rm D}(h,\lambda_1)$ profile for this altitude region are realistic.

Above the tropopause, up to 25 km, the coefficients are larger than those derived for the 1964 Attenuation Model by a factor of about 20 (at 20 km for λ_1 = 0.55 μ). This difference may be attributed in part to the intrinsic difficulties of converting a size distribution to an optical parameter, that is, establishing the radii limits, particle shape, chemistry, and index of refraction. Relative to profile shape, a turbidity maximum dominates at about 19 km (Figure 8). The measurements of Rosen (1968) and those of Volz (1968) for 1964 to 1968 are in satisfactory agreement

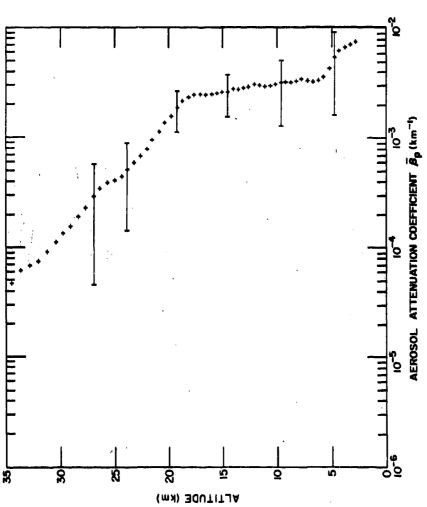


Figure 7. Mean of 79 Low Stratospheric Dust Profiles (Table 3) for April 1964 to April 1965. Aerosol attenuation coefficients, $\hat{\beta}_{p}(h,\lambda_{1})$; standard deviation limits attributable to error and atmospheric variations; $\lambda_{1}=0.55\mu$; +++++measurements with searchlight probing

Figure 8. Mean Turbidity Profile, $\bar{\beta}_{p}(h,\lambda_{1})/\beta_{r}(h,\lambda_{1})$ (See caption for Figure 7)

with the mean optical thickness and shape of the Group (B+C+D) profiles. Table 3. Also their results show that the stratospheric dust level has remained approximately constant from 1964 to the time of this writing. The $\tilde{\beta}_p(h,\lambda_1)$ curve (Figure 7) shows this dust feature as the knee of the profile rather than a massive layer feature indicated by the turbidity profile. This conceptual relationship suggests that over-emphasis is possible when dealing only with turbidity profiles.

The turbidity profile shows an upper stratospheric maximum with its lower terminus at 25 km. This altitude then, was the basis for choosing the upper stratospheric dust limit in Eq. (7). The maximum at 26 km occurs with sufficient frequency to be easily identified in the turbidity profile. The existence of such an aerosol concentration above 20 km is supported by the analysis of satellite photography reported by Mateer, Dave, Dunkelman, and Evans (1967).

To establish upper altitude aerosol coefficients, a least square fit was computed for $\hat{\beta}_p(h,\lambda_1)$ from 26 to 32 km (Figure 9). The result, $H_p=3.75$ km (in effect derived from 790 measurement points), was used in Eq. (8) to extend the values to 50 km. Miller (1967) obtained $H_p=3.25$ km from a thorough analysis of rocket measurements acquired in 1964 for this altitude region. The overall profile from sea level to 50 km is presented in Figure 10 (Table 4.11). Since the

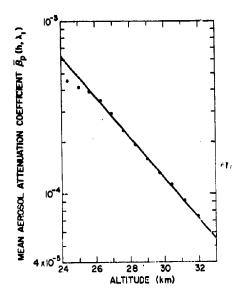


Figure 9. Expanded Scale for 26 to 32 km Altitude Region Showing H_p = 3.75 km for 79 Profile Mean; Aerosol Attenuation Coefficients, $\beta_p(h,\lambda_1)$ vs Altitude; Least Square Fit Used to Extrapolate to 50 km; λ_1 = 0.55 μ

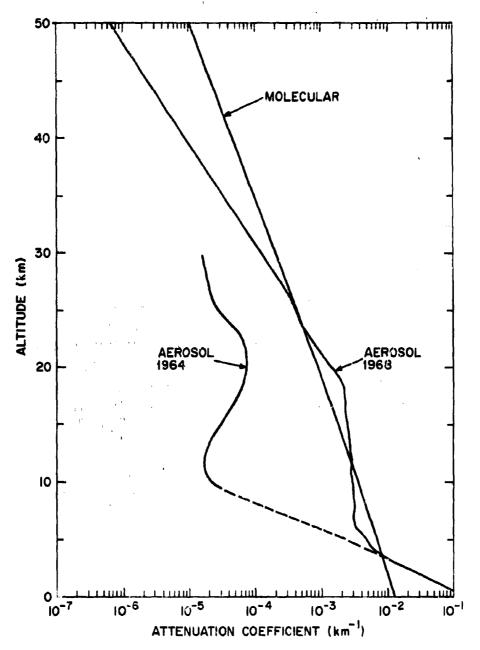


Figure 10. Comparison of Profiles. Aerosol attenuation coefficients $\beta_p(h, \lambda_1)$, with molecular $\beta_r(h, \lambda_1)$. The 1964 profile shows interpolation between 5 to 10 km; λ_1 = 0.55 μ

turbidity is proportional to the mixing ratio, the diminishing values for the extrapolation imply the acrosol source exists below 30 km. Should the source be of meteoric origin, the mixing ratio would tend to be constant or increase for altitudes 30 to 50 km.

Thus far we have selected a set of measurements for $\lambda_1=0.55\mu$ and provided reasons for its use. It would be in order now to examine some expressions leading to corresponding aerosol profiles for other wavelengths. If we consider a real atmosphere, the aerosol sizes within unit volume can be described by a size distribution function, ψ (r). Various size distribution functions are in use: the Junge type power law (1963) with a choice of exponents discussed in detail by Bullrich (1964), a similar distribution modified by gaps observed by Fenn (1964), a log-Gaussian distribution used by Foitzik (1965), a composite distribution with components from several types. The optical-particle size relationship utilizes ψ (r) such that

$$\beta_{p}(m,r,\lambda) = \int_{N_{r_2}}^{N_{r_1}} \sigma_{p}(m,r,\lambda) dN_{p}(r) , \qquad (9)$$

$$dN_{p} = N_{o} \psi(r) dr , \qquad (10)$$

$$N_{o}(h) = C N_{p}(h) . (11)$$

 eta_p is the aerosol attenuation coefficient, m is the index of refraction, N_{r_1} and N_{r_2} are the aerosol number density limits established by the radii limits r_1 and r_2 , σ_p is the aerosol cross section for each particle, N_p is the total number of particles between r_1 and r_2 . For a given altitude, N_o actually is proportional to the particle number density between r_1 and r_2 . Since the same size distribution function applies to all altitudes (an assumption), Eqs. (9), (10), and (11) are combined

$$\beta_{p}(h,\lambda) = CN_{p}(h) \int_{r_{1}}^{r_{2}} \sigma_{p}(r,\lambda) \psi(r) dr$$
 (12)

Here, $CN_p(h)$ is placed outside the integral which now contains only factors that are independent of altitude; also, m is removed because subsequent considerations will pertain to particles without any distinction in refractive index. If Eq. (12) is normalized to sea level conditions, the integral cancels out. Then generally for the various wavelengths λ , and specifically for $\lambda_1=0.55\mu$, we have

$$\frac{\beta_{\mathbf{p}}(\mathbf{h},\lambda)}{\beta_{\mathbf{p}}(\mathbf{0},\lambda)} = \frac{\beta_{\mathbf{p}}(\mathbf{h},\lambda_{1})}{\beta_{\mathbf{p}}(\mathbf{0},\lambda_{1})} = \frac{N_{\mathbf{p}}(\mathbf{h})}{N_{\mathbf{p}}(\mathbf{0})}$$
(13)

or

$$\beta_{\mathbf{p}}(\mathbf{h},\lambda) = \frac{\beta_{\mathbf{p}}(\mathbf{0},\lambda)}{\beta_{\mathbf{p}}(\mathbf{0},\lambda_{1})} \cdot \beta_{\mathbf{p}}(\mathbf{h},\lambda_{1}) . \tag{14}$$

Equation (13) has been derived in this manner to demonstrate its compatibility with particle size considerations. Sea level conditions have been researched extensively by Curcio and Durbin (1959), Curcio, Knestrick, and Cosden (1961), Knestrick, Cosden, and Curcio (1961), Dunkelman (1952), Baum and Dunkelman (1955). The $\beta_p(0,\lambda)$ values for a 25 km M.R., based on the results of these authors, are shown in Figure 11 (see also Elterman, 1964). Utilizing these results, in conjunction with the $\hat{\beta}_p(h,\lambda_1)$ profile (Table 4.11), all requirements for the right-hand side of Eq. (14) are satisfied and an array of aerosol attenuation coefficients can be computed for all altitudes and wavelengths of interest.

The aerosol optical thickness from sea level to altitude h, $\tau_p(h, \lambda)$, and the aerosol optical thickness from some altitude h to space, $\tau_p^*(h, \lambda)$, are included in the model tabulations. The expressions for deriving these parameters have the same form as Eqs. (4) and (5).

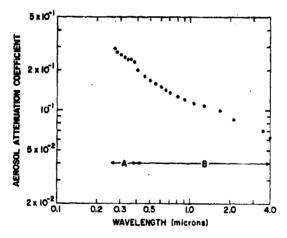


Figure 11. Aerosol Attenuation Coefficients $\beta_{\rm D}(0,\lambda)$ vs Wavelength at Sea Level for a Meteorological Range Approximating 25 km. A – derived from Baum and Dunkelman (1955) B – contained in Curcio, Knestrick, and Cosden (1961)

5. ATMOSPHERIC EXTINCTION

In this section, three sets of extinction parameters are considered; extinction coefficient, extinction optical thickness from sea level to a desired altitude, and extinction optical thickness from a desired altitude to space.

The atmospheric extinction coefficient $\beta_{\rm ext}$ is the sum of all the attenuating components:

$$\beta_{\text{ext}}(h,\lambda) = \beta_{\text{r}}(h,\lambda) + \beta_{3}(h,\lambda) + \beta_{p}(h,\lambda)$$
 (15)

The extinction optical thickness from sea level to altitude h, $\tau_{\rm ext}(h,\lambda)$, and the extinction optical thickness from some altitude h to space, $\tau_{\rm ext}^{i}(h,\lambda)$, are included in the tabulations of the attenuation model. The expression for deriving these parameters has the same form as Eqs. (4) and (5).

6. EXPLORATORY TRANSMISSION CALCULATIONS

Using the derived tabulations that follow, some exploratory calculations with extinction parameters (for any of the wavelengths) are demonstrated. Rayleigh, aerosol, and ozone parameters can be used similarly.

For horizontal transmission (T_h) over a path (d) at any altitude (h) , the extinction coefficient

$$T_{h} = \exp \left[-\beta_{\text{ext}}(h,\lambda) \cdot d \right]. \tag{16}$$

For vertical and slant-path transmission from sea level to a given altitude, at zenith angle θ for all wavelengths of interest

$$T_{c-h} = \exp \left[-\tau_{ext}(h) \cdot \sec \theta \right] . \tag{17}$$

For vertical and slant-path transmission between two altitudes above sea level

$$T_{\Delta h} = \exp - \left[\tau_{\text{ext}}(h_2) - \tau_{\text{ext}}(h_1) \right] \cdot \sec \theta . \tag{18}$$

For vertical and slant-path transmission from a given altitude out into space

$$T_{h=\infty} = \exp \left[-\tau_{\text{ext}}^{\dagger}(h) \sec \theta \right] . \tag{19}$$

7. CONCLUDING REMARKS

The procedure for developing the aerosol attenuation profile is summarized as follows:

- Various studies were compared and of these a set of measurements selected.
- (2) The choice of measurements (comprising 119 profiles from 2.76 to 34.4 km) was examined statistically. This resulted in the elimination of 40 profiles (December 1963 to March 1964 inclusive) characterized by a high volcanic dust component.
- (3) The mean of the 79 remaining profiles was extended to sea level and to 50 km respectively by reasonably supported extrapolations.
- (4) The overall profile then was developed laterally to obtain 21 additional profiles for the wavelengths of interest.

A significant aspect of the procedure is that the wavelength-height array of parameters was derived independently of the assumptions associated with conversion of a size distribution to an optical parameter.

For most purposes, calculations using the new parameters will be affected only moderately. For example at $\lambda_1=0.55\mu$, the 1964 Attenuation Model provides an extinction optical thickness, $\tau_{\rm ext}=0.331$, for a vertical air mass. The new parameters yield $\tau_{\rm ext}=0.379$, resulting in a transmission change of about 3-1/2 percent. However, for long path horizontal transmission calculations above 5 km and for long slant-path calculations entailing large zenith angles, the new aerosol parameters can function more significantly.

As mentioned previously, the Rayleigh and ozone parameters are unchanged.

8. TABULATION OF PARAMETERS

Tables 4.1 to 4.22, which follow, comprise the atmospheric attenuation model. Exponents are in computer notation; for example, read $2.86-3=2.86\times10^{-3}$ and 2.86 3 as 2.86×10^{3} .

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7	1- 005-1	-354	1.291	5-13 -2	-279	-147	3-11-5	069	35-125	5.22 -1	1.323	36.308	
ED .	1-444	20°	1-133	2- 51-2	916	111	1- 69-7	1 220	34.586		2.206	35.685	
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· ·	1-121-1		76.9	6.05 -3	350	770	2.20	1-698	34-119	3.40	2.926	34-965	
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. 0	7-626 -2	\$1:1	.531	5-55 -3	.367	090	2-98 -1	2-440	33.376	3-78 -1	3-952	33.939	
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1.600 - 3 1.212	1.600 - 3 1.211	3 5		1.209	510	7 25-1	014		7- 11- A	7.054	55.4	8-21 -2	4-576	72.
1.366 -3 1.212 .009 9.22 -5 .411 .000 5.88 -2 3.092 .320 6.02 -2 4.773 .2146 .266 5.02 -2 4.773 .2146 .266 5.02 -2 4.773 .2146 .266 5.02 -2 4.773 .2146 .266 5.02 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.46 -2 4.885 .2240 4.885 .2240 4.885 .2240 4.885 .2240 4.885 .2240	1366 -3 1.212 009 9.22 -5 .411 000 5.88 -2 3.092 320 5.02 -2 213 008 7.06 -5 .411 000 4.90 -2 3.146 266 266 266	32		1,211	.011	1-20 -4	174-	000	7- 68-9	5.029	-38¢	7-00-1	4-652	.395
1.167 -3 1.213 .008 7.06 -5 .411 .000 4.90 -2 5.146 .266 5.02 -2 4.773 9.990 -4 1.214 .007 5.41 -5 .411 .000 4.35 -2 3.194 .220 4.46 -2 4.820 1.930 -4 1.215 .006 4.15 -5 .411 .000 3.05 -2 3.233 .180 3.18 -5 .411 .000 3.05 -2 3.236 .140 3.13 -2 4.861 1.77 -2 4.861 1.200 -4 1.217 .005 2.44 -5 .411 .000 2.55 -2 3.264 .119 2.62 -2 4.924 1.19 2.62 -2 4.924 1.217 .005 2.44 -5 .411 .000 2.55 -2 3.348 .095 2.62 -2 4.924 1.19 2.62 -2 4.924 1.218 .005 1.218 .000 1.26 -2 3.355 .057 1.23 -2 4.969 4.777 -4 1.218 .004 1.09 -5 .411 .000 1.20 -2 3.355 .057 1.25 -2 4.969 4.777 -4 1.218 .002 2.55 -9 .411 .000 1.20 -2 3.369 .027 1.25 -2 4.969 1.20 1.219 .002 2.55 -9 .411 .000 2.39 -3 3.360 .033 2.777 1.35 -2 5.012 2.25 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.390 .033 9.71 -3 5.012 2.25 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.395 .013 4.74 -3 5.037 1.75 -4 1.220 .001 1.220	1.167 -3 1.213 .008 7.06 -5 .411 .000 4.90 -2 5.146 .266 5.02 -2 5.990 -4 1.214 .007 5.41 -5 .411 .000 4.35 -2 3.193 .220 4.46 -2 5.990 -4 1.215 .006 4.15 -5 .411 .000 3.05 -2 3.233 .180 3.74 -2 5.41 .006 2.55 -2 3.234 .180 3.74 -2 5.41 .000 2.55 -2 3.286 .147 3.13 -2 5.42 .4 5 .4 5 .4 5 .4 5 .4 5 .4 5 .4	33	1.366 -3	1.212	600-	9-55 -5	114.	000•	5.88 -2	3.092	.320	7- 70-9	4.717	.330
9.990 -4 1.214 .007 5.41 -5 .411 .000 4.35 -2 3.793 .220 4.466 -2 4.820 4.466 -2 4.820 4.466 -2 4.820 4.466 -2 4.823 .184 2.74 -2 4.861 1.215 .006 4.15 -5 .411 .000 3.05 -2 3.233 .184 2.74 -2 4.861 1.217 .005 2.44 -5 .411 .000 2.50 -2 3.294 .119 2.62 -2 4.924 6.335 -4 1.217 .005 2.44 -5 .411 .000 2.50 -2 3.394 .075 1.22 4.924 7.717 -4 1.218 .004 1.54 -5 .411 .000 1.26 -2 3.318 .075 1.53 -2 4.924 7.717 -4 1.218 .004 1.09 -5 .411 .000 1.20 -2 3.355 .057 1.58 -2 4.924 7.717 -4 1.219 .002 2.50 -4 11 .000 1.20 2.349 .025 1.51 -3 5.012 2.566 -4 1.219 .002 2.41 .000 9.39 -3 3.395 .037 1.24 -5 5.012 2.566 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.395 .013 6.05 -3 5.021 2.523 -4 1.220 .002 2.88 -6 .411 .000 4.50 -3 3.404 .009 3.74 -3 5.031 1.220 .001 1.220 .001 1.220 .001 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 2.23 -4 1.220 .001 1.220 .001 2.23 -4 1.220 .001 2.20 -2 2.20 2.20 2.20	9.990 -4 1.214 .007 5.41 -5 .411 .000 4.35 -2 3.193 .220 4.446 -2 8.567 -4 1.215 .006 4.15 -5 .411 .000 3.65 -2 3.233 .180 3.18 .180 3.18 .220 4.18 .220 1.19 .220 1.220 1.221 .006 4.15 .200 2.50 -2 3.256 .147 3.13 .226 .2 2 3.256 .147 3.13 .220 .220 1.217 .006 1.56 -5 .411 .000 2.50 -2 3.259 .119 2.62 -2 2 5.451 .000 1.219 .2 3.318 .095 2.25 .2 2 3.356 .075 1.58 .2 2 2 3.356 .0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	*		1.213	800-	7-06 -5	114-	00n	4.90 -2	3. [46	•566	2-65	4-173	-475
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6.35	6.335 -4 1.217 .005 2.44 -5 -411 .000 2.55 -2 3.294 .119 2.66 -2 5.411 .000 2.19 -2 3.318 .095 2.45 -2 5.411 .000 2.19 -2 3.318 .095 2.45 -2 5.411 .000 1.54 -2 3.318 .095 2.45 -2 5.411 .000 1.54 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 3.355 .005 1.58 -2 2.25 -2 3.355 .005 1.58 -2 2.25 -2 3.355 .005 1.58 -2 2.25 -2 3.355 .005 1.58 -2 2.25 -2 3.355 .005 1.58 -2 2.25 -2 3.355 .005 1.55 -2 2.25 -2 3.355 .005 1.55 -2 2.35 1.55 -2 3.355 .005 1.55 -2 2.25 -2 3.355 .005 1.55 -2 2.35 1.55 -2 2.355 .005 1.55 -2 2.35 1.55 -2 2.355 .005 1.55 -2 2.35 1.55 -2 2.355 .005 1.55 -2 2.35 1.55 -2 2.35 1.55 -2 2.35 1.55 1.55 -2 2.35 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1	35	8-567 -4 -4-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-	1.215	9 10	6- CT-4	114.	200	3.05	3.233	751	2- 61-7	1004	24.
5.461 4 1.217 .004 1.66 -5 .411 .000 2.19 -2 3.318 .095 2.25 -2 4.948 4.717 4 1.218 .004 1.45 -5 .411 .000 1.88 -2 3.318 .095 2.25 -2 4.949 4.717 4 1.218 .004 1.45 -5 .411 .000 1.86 -2 3.355 .057 1.58 -2 4.949 4.947 1.219 .003 1.09 -5 .411 .000 1.26 -2 3.355 .057 1.58 -2 4.949 4.947 1.219 .002 6.40 -6 .411 .000 1.20 -2 3.369 .044 1.24 -2 5.001 2.35 1.58 -2 4.949 4.947 .002 2.38 -6 .411 .000 5.82 -3 3.360 .033 9.71 -3 5.012 2.32 -4 1.220 .001 1.220 .001 1.221 .000 4.90 -4 1.210 .000 4.39 -3 3.404 .009 4.71 -3 5.034 1.767 -4 1.220 .001 1.265 -6 .411 .000 2.42 -3 3.404 .009 3.74 -3 5.037 1.312 .4 1.220 .001 1.29 -6 .411 .000 2.42 -3 3.407 .000 2.98 -3 5.041 1.312 .4 1.220 .001 1.29 -6 .411 .000 2.24 -3 3.407 .000 2.98 -3 5.041 1.312 .4 1.220 .001 1.29 -6 .411 .000 1.88 -3 3.410 .003 2.39 -3 5.045 1.312 .4 1.321 .001 2.39 -3 3.410 .001 2.39 -3 5.045	5.461 4 1.217 .004 1.66 -5 .411 .000 2.19 -2 3.318 .095 2.25 -2 4.11 .000 1.68 -2 3.336 .075 1.93 -2 4.000 1.54 -2 3.355 .057 1.93 -2 4.000 1.54 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.28 .003 1.24 -2 3.355 .057 1.25 -2 3.355 .057 1.25 -2 3.355 .057 1.25 -2 3.355 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 1.25 .057 .05 .057 1.25 .0		97 972 7	1.2.1		5- 44-7	114	000	7 05 7	307.5	01	3	4.9.4	17.5
4.717 + 1.218 .004 1.43 -5 .411 .000 1.56 -2 3.356 .057 1.58 -2 4.967 4.080 -4 1.218 .003 1.09 -5 .411 .000 1.54 -2 3.355 .057 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 4.967 1.58 -2 1.219 .002 6.40 -6 .411 .000 9.39 -3 3.386 .025 7.79 -3 5.012 2.321 -4 1.220 .002 3.75 -6 .411 .000 5.42 -3 3.386 .013 6.05 -3 5.034 1.767 -4 1.220 .001 2.21 -6 .411 .000 2.62 -3 3.400 .013 4.71 -3 5.037 1.55 -4 1.220 .001 1.25 -6 .411 .000 2.62 -3 3.410 .009 2.98 -3 5.041 1.324 -4 1.220 .001 1.25 -6 .411 .000 2.26 -3 3.410 .000 2.39 -3 5.041 1.220 .001 1.220 .411 .000 2.26 -3 3.410 .001 2.39 -3 5.045 1.221 .001 2.22 -6 .411 .000 1.88 -3 3.410 .001 2.39 -3 5.045	4.717 -4 1.218 .004 1.43 -5 .411 .000 1.54 -2 3.356 .075 1.93 -2 4.080 -4 1.218 .003 1.09 -5 .411 .000 1.54 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.58 -2 3.355 .057 1.59 -3 3.355 .057 1.59 -3 3.355 .057 1.59 -3 3.355 .057 1.59 -3 3.355 .057 1.59 -3 3.355 .057 1.55 .057 1.55 .057 1.55 .057 1.55 .057 1.55 .057 1.55 .057 .057 1.55 .057 .057 1.55 .05	0 0	194.5	1.217	460	1.86 -5	114	000		4.418	8	7- 57-7	4.048	660
4.080 -4 1.218 .004 1.09 -5 .411 .000 1.54 -2 3.355 .057 1.58 -2 4.987 3.535 -4 1.219 .003 8.36 -6 .411 .000 1.20 -2 3.369 .044 1.24 -2 5.001 3.688 -6 1.219 .002 4.90 -6 .411 .000 7.51 -3 3.348 .025 779 -3 5.021 2.521 -6 1.220 .002 3.75 -6 .411 .000 5.82 -3 3.395 .018 6.05 -3 5.028 2.523 -6 1.220 .002 2.21 -6 .411 .000 5.82 -3 3.400 .013 6.05 -3 5.034 1.767 -6 1.220 .001 2.21 -6 .411 .000 2.62 -3 3.400 .013 4.71 -3 5.034 1.575 -6 1.220 .001 1.269 -6 .411 .000 2.62 -3 3.400 .013 2.74 -3 5.031 1.575 -6 1.220 .001 1.220 .001 2.22 -3 3.410 .009 2.98 -3 5.041 <	4.080 -4 1.218 .003 1.09 -5 .411 .000 1.54 -2 3.355 .057 1.58 -2 3.535 -4 1.219 .003 8.36 -6 .411 .000 1.20 -2 3.369 .044 1.24 -2 3.668 -4 1.219 .002 .411 .000 1.20 -3 3.380 .023 17.1 -3 2.321 -4 1.220 .002 3.75 -6 .411 .000 5.62 -3 3.395 .013 6.05 -3 2.321 -4 1.220 .002 2.411 .000 5.62 -3 3.400 .013 6.05 -3 1.767 -4 1.220 .001 2.21 -6 .411 .000 2.42 -3 3.404 .009 4.76 -3 1.333 -4 1.220 .001 1.26 -0 .411 .000 2.42 -3 3.404 .009 2.36 -3 1.333 -4 1.220 .001 1.29 -0 .411 .000 2.22 -3 3.404 .009 2.39 -3 1.212 -4 1.220 .001 1.220 -6 .411 .000 2.25 -3 3.410 .001	, 0	4-717-4	1-218	400	1.43 -5	-411	000	1-88 -2	3.338	50.	7- 66-1	4.969	-078
3-535 -4 1.219 .003 8.36 -9 .411 .000 1.20 -2 3.369 .044 1.24 -2 5.001 3-068 -4 1.219 .002 6.40 -6 .411 .000 9.39 -3 3.360 .033 9.71 -3 5.012 2-366 -4 1.220 .002 3.75 -6 .411 .000 5.82 -3 3.395 .018 6.05 -3 5.028 2.321 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.400 .013 4.71 -3 5.033 1.767 -4 1.220 .001 2.21 -6 .411 .000 2.62 -3 3.400 .003 3.77 -3 5.031 1.554 -4 1.220 .001 1.29 -6 .411 .000 2.26 -3 3.410 .009 2.39 -3 5.041 1.312 -4 1.220 .001 0.20 -411 .000 1.88 -3 3.410 .003 2.39 -3 5.045	3-535 -4 1.219 .003 8.36 -9 .411 .000 1.20 -2 3.369 .044 1.24 -2 3.668 -4 1.219 .002 6.40 -6 .411 .000 9.39 -3 3.380 .033 9.71 -3 2.666 -4 1.220 .002 3.75 -6 .411 .000 7.51 -3 5.395 .013 2.521 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.400 .013 6.05 -3 1.767 -4 1.220 .001 1.221 -6 .411 .000 2.42 -3 3.400 .013 1.554 -5 1.220 .001 1.25 -6 .411 .000 2.42 -3 3.400 .003 1.373 -4 1.220 .001 1.22 -6 .411 .000 2.42 -3 3.410 .000 2.39 -3 1.212 -4 1.221 .001 9.91 -7 .411 .000 2.25 -3 3.412 .001 2.39 -3	14	4-080-4	1.218	.003	1.09 -5	114.	•000	1.54 -2	3,355	-057	7- 85-1	4-987	190-
3.068 -4 1.219 .002 6.40 -6 .411 .000 9.39 -3 3.380 .033 9.71 -3 5.012 2.466 -4 1.219 .002 4.90 -6 .411 .000 7.51 -3 5.388 .025 7.79 -3 5.021 2.466 -4 1.220 .002 2.88 -6 .411 .000 5.82 -3 3.490 .013 6.05 -3 5.033 2.523 -4 1.220 .002 2.88 -6 .411 .000 3.57 -3 3.400 .013 4.71 -3 5.033 1.767 -4 1.220 .001 1.269 -0 .411 .000 2.42 -3 3.407 .000 2.98 -3 5.041 1.373 -4 1.220 .001 1.29 -6 .411 .000 2.26 -3 3.410 .003 2.39 -3 5.041 1.212 -4 1.220 .001 1.29 -6 .411 .000 1.88 -3 3.412 .003 2.39 -3 5.045	3.068 -4 1.219 .002 6.40 -6 .411 .000 9.39 -3 3.360 .033 9.71 -3 2.666 -4 1.219 .002 4.90 -6 .411 .000 7.51 -3 3.368 .025 7.79 -3 2.321 -4 1.220 .002 2.88 -6 .411 .000 4.50 -3 3.400 .013 6.05 -3 2.523 -4 1.220 .001 2.21 -6 .411 .000 3.57 -3 3.400 .013 6.71 -3 1.767 -4 1.220 .001 1.69 -0 .411 .000 2.42 -3 3.407 .009 3.74 -3 1.373 -4 1.220 .001 1.29 -6 .411 .000 2.25 -3 3.410 .003 2.39 -3 1.212 -4 1.221 .001 9.91 -7 .411 .000 1.88 -3 3.412 .001 2.00 -3	74	3.535 -4	1.219	.003	8-36 -6	-411	000*	7- 07-1	3.369	***	1-54	100-5	945
2.666 -6 1.219 .002 6.90 -6 .411 .000 7.51 -3 5.388 .025 7.79 -3 5.021 2.321 -4 1.220 .002 3.75 -6 .411 .000 5.82 3.395 .018 6.05 -3 5.028 2.523 -4 1.220 .002 2.88 -6 .411 .000 4.50 -3 5.404 .009 3.74 -3 5.033 1.767 -4 1.220 .001 1.69 -0 .411 .000 2.42 -3 5.404 .009 3.74 -3 5.037 1.354 -4 1.220 .001 1.29 -6 .411 .000 2.42 -3 5.407 .00 2.98 -3 5.404 1.212 -4 1.220 .001 1.29 -6 .411 .000 1.88 -3 5.407 .00 3.5.445 1.212 -4 1.220 .001 1.29 -6 .411 .000 2.25 -3 5.407 .00 3.5.445	2.666 -6 1.219 .002	43	3-068 -4	1.219	700.	9-04-9	-411	000-	9-39 -3	3-390	-033	9.71 -3	5.012	.035
2.22.4 1.220 .002 2.75 6 .411 .000 4.50 -3 3.555 .016 8.02 5.5033 2.22.3 -4 1.220 .002 2.88 -6 .411 .000 4.50 -3 3.400 .013 4.71 -3 5.033 1.767 -4 1.220 .001 1.69 -0 .411 .000 2.42 -3 3.404 .009 3.74 -3 5.037 1.554 -4 1.220 .001 1.69 -0 .411 .000 2.42 -3 3.407 .000 2.98 -3 5.041 1.212 -4 1.220 .001 1.29 -6 .411 .000 2.25 3 3.410 .003 2.39 -3 5.043 1.212 -4 1.221 .001 2.99 -7 .411 .000 1.88 -3 3.412 .001 2.90 -3 5.045	2.521 -4 1.220 .002 2.88 -6 .411 .000 4.550 -3 3.400 .013 4.71 -3 1.757 -4 1.220 .001 1.659 -0 .411 .000 4.557 -3 3.400 .013 4.71 -3 1.757 -4 1.220 .001 1.699 -0 .411 .000 2.62 -3 3.407 .000 2.98 -3 1.554 -4 1.220 .001 1.29 -6 .411 .000 2.62 -3 3.410 .000 2.99 -3 1.212 -4 1.221 .001 2.29 -6 .411 .000 1.68 -3 3.410 .003 2.39 -3 1.212 -4 1.221 .001 2.22 -3 3.412 .001 2.00 -3	4 4	2.666 -6	1.219	700-	4.90 · 6	-411	000	7.51 -5	4. 586	20.0	5- 63- 4	170-6	200
2.525 - 1.520 .002 .2.56 - 11 .000 4.50 - 5 5.400 .003 4.76 - 5 5.037 1.767 - 1.220 .001 .2.21 - 6 .411 .000 2.62 - 3 5.407 .000 2.76 - 5 5.041 1.575 - 1.220 .001 1.29 - 6 .411 .000 2.25 - 3 3.410 .003 2.39 - 3 5.043 1.212 - 4 1.221 .001 9.91 - 7 .411 .000 1.88 - 3 3.412 .001 2.00 - 3 5.045	2.525 -4 1.220 .002 2.58 -6 .411 .000 3.57 -3 3.404 .009 3.74 -3 1.254 -4 1.220 .001 1.269 -0 .411 .000 2.62 -3 3.407 .009 2.98 -3 1.554 -4 1.220 .001 1.29 -6 .411 .000 2.25 -3 3.410 .003 2.39 -3 1.212 -4 1.220 .001 0.991 -7 .411 .000 1.68 -3 3.412 .001 2.00 -3	Ç:	17677	077-1	700-	3-17-0	77.	999	2000	0.040	970		3.028	410
1.557 - 1.520 .001 2.21 2.00 2.35 - 3.540 .003 2.37 - 3.550	1.554 -4 1.220 .001 1.69 -0 .411 .000 2.62 -3 3.407 .009 2.98 -3 1.554 -4 1.220 .001 1.69 -0 .411 .000 2.65 -3 3.407 .000 2.98 -3 1.212 -4 1.220 .001 1.29 -6 .411 .000 2.25 -3 3.410 .003 2.39 -3 1.212 -4 1.221 .001 9.91 -7 .411 .000 1.88 -3 3.412 .001 2.00 -3	9 !	2-523	022-1	700*	9- 99-7	114.	000-	00.	304.6	510.	C	0000	
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1.2.14 1.2.2001 1.9.44.1 .000 1.88 -5 3.4.2 .001 2.0.16.0.	1.212 -4 1.221 .001 9.91 -7 .411 .000 1.88 -5 3.412 .001 2.00 -3	6 4	4- 460-7	220	100	01 50°1		000	2.06 -1	207.4	800	1 0r · 2	140.4	1
		, 6	4 (1)	1000	100	9-91 -7	114	000	1.88 -5	714-4	100	7-00-7	5.045	700

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4	1 2	, r	T.	o d	7 g	, 'g'	. E	. T.	r3	Pert .	re in	֞֞
0	1-060-1	00.	-927	2.50 -1	000-	.395	3-70 -8	000	-303 -303	7.7	00.	1.628
• ^	7- 206-6	3 5	128	4-75 -2	. 190	217•	6- 64-7	900	35	7 97 1	997	7.7
, 197	8-148 -2	285	249	1-39 -2	292	103	2007	900	262	7	586	1-0-1
•	7	-362	.565	1-05 -2	-308	-088	2-03 -3	010	•293	8-60-2	.681	196
•		-432	-495	7.94 -3	-317	-078	1.98 -3	-012	167*	7-59	.762	-866
•		.495	.433	5-60 -3	.324	•072	1.94 -3	+10-	687*	6-67 -2	.833	\$4.
_		.550	.377	5.21 3	.329	-066	2-00-3	•016	-287	6-01 -2	169.	.731
c	4.712 -2	909	.327	5-36 -3	- 334 -	190-	Z-05 -3	910-	-285	5-45 -4	+36*	-674
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13		.775	.152	4-20 -3	.359	•036	7.59 -3	039	-265	3-60 -2	1-174	**
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91		-832	-095	3-99 -3	-372	• 073	9-25 -3	.065	.239	7- 85-7	1-270	.356
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5 *	4-205 -5	906	. 027	7-80 -	392	•003	1-73 -2	.178	<u>.16</u>	2-52-2	1.471	-156
52	3-592 -3	\$06.	-024	5-57 -4	.392	-003	1-62 -2	195	87T	7.04 -2	1-493	.135
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31	1.415 -3	816*	.010	1-51 -4	.395	100-	7-12 -3	. 263	140-	8-69-3	1.577	.051
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1 11	(0-1)	(h - e)	•	(4-0)	(* - *	(f. mg)	(Q-P)	(F) - 80	(fcm ⁻¹)	(q-0)	(B - 8)
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6-060 -2	*90*	105"	1-96-1	.173	702.	5-87 -6	000	100-	1-99-1	-236	-709
5-487 -2	171-	-443	4.56 -2	-248	.131	5-27 -6	000	100-	7- 00-7	.370	-575
4-957 -2	.173	.391	7- 16-1	.281	660	4.50 4	900	100.	6-87 -2	4.	169
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4.015 -2	-263	-301	7-63 -3	-304	-075	3.98	900	100-	7- 82.4	-501	975
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5-669 -3	-528	-036	3.08 -3	-363	110-	5- 95-7	9	000	8-78 -3	-837	940
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7.454 -5 .449 .401 2.55 -6 .364 .000 0000 .000 7.71 -5 . 5.756 -5 .449 .001 1.95 -6 .364 .000 0000 .000 6.70 -5 . 5.756 -5 .450 .000 1.50 -6 .364 .000 0000 .000 5.88 -5 . 5.056 -5 .450 .000 1.14 -6 .344 .000 0000 .000 .5.17 -5 .		ŗ		3-32 -6	.364	8	ċ	900·	000-	8.88	÷8.	on.
6.508 -5 .449 .001 1.95 -6 .354 .000 U000 .000 6.70 -5 . 5.726 -5 .450 .000 1.50 -6 .364 .000 U000 .000 .000 5.84 -5 . 5.056 -5 .450 .000 1.14 -6 .3*4 .000 0000 .000 .517 -5 .		ŗ		2-55 -6	-364	000-	•	000	900-	7.71 -5	-814	100.
5.726 -5 .450 .000 1.50 -6 .364 .000 0000 .000 5.08 -5 . 5.056 -5 .450 .000 1.14 -6 .3 ² 4 .000 0000 .000 .517 -5 .		ψ.		1.95 -6	-304	000	j	000	000	6-70 -5	**	20.
5.056 -5 .450 .000 1-14 -6 .344 .000 0000 .000 .000 .5-17 -5		ıçı ı		1.50 -6	.364	000-	9	000	000	S-88-5	+19.	ž į
1 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		'n		9- +T•T		9			٤		4	

Table 4.8 Parameters at 0.40 microns

1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	Alt.	Rayleigh	Kayleigh	Kayleigh	Acrosol								
		atten.	optical	optical	atten.	optical	optical	absorp.	optical	optical	coeff.	popolo	optical
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	ĵį	coeff. (km ⁻¹)	(0 - b)		00eff. (km ⁻¹)	9 EK (2) EK (3) EK (4) EK (4) EK (4) EK (5) EK (5) EK (6) EK (6) EK (7)	(h - 8)	(Fm 1)	(A)	mck. (h - se)	(km ⁻¹)	4 0 0	(h - e.)
1, 10, 10, 10, 10, 10, 10, 10, 10, 10,	.	ec,	r,	i Ne	80,00	h ^Q	, n	B3		13	Bent	'an	.r.
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	,	4.303 -2	000	156	2-00 -1	000	.316	9	98.	900.	2-43 -1	999	.050
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	-	3-905 -2	740-	.323	8-80 -2	*1.	-172	ð	000	000-	1-27 -1	. 195	-455
1,114	~	3-536 -2	-073	- 585	3-80	-207	-109	3	600	900	7.33 -2	-285	555
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	m .	3-194 -2	-115	-252	1.59 -2	467.	-082	d	9	9	7- P	945	
1,100		9 6	741-	177	0.4% 1.3 2.4 3.5 4.3	354		.	9	3 8	3.22	27	7.7
1,000	v 1		60	667	6-50-5	-624	-050	3 6	000	900	2-11-2	453	727
1,000	۰.		710	941	4.14	26.2		d	000	900	2.6	479	777
1,453 - 2, 25	_ «		24.45	871	£- 53 -3	267	0 40	d	900	39	7-87-7	503	1117
1,281 - 2			- 553	111	f- 11-4	-272	\$	6	000	200	2-69-7	.525	-156
1,281 2 284 1082 3,78 3, 284 1083 1			-258	-095	F- 10*+	-276	040	ó	000	. 00.	7- 91-1	¥s.	-136
1,006 -1 . 204 . 0.00 .	_		-282	-082	3.76 -3	-280	-037	•	000	300	1.66 -2	-562	111
\$ 1,185 - 1,196 - 1,19	~		•53•	.070	3.95 -3	.283	•033	•	000	3	7-64-1	. 378	507-
6.844 - 3.312	~		*30¢	090.	3.65 -3	.287	670-	.	000	20.	7-08-1	-592	.069
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	•		-312	.051	3.57 -3	162-	•025	•	000	000	1.16 -2	000	9/0
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\$\begin{array}{c} \text{A_173}	۰	ı.	•326	.037	3-19 -3	- 298	670	ċ	3	300	5:	***	600
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1.592 - 3 - 354	6 0 4		346.	.027	2-05	500	210.	.	3	38			
1,000 1,00	.		045.	670.	£-21-7	106.	200	.		3	7 7 7 7	100	100
1, 201	٠.		***	200	1 27 1 2	4.564		3 4	98	3 6	10.4	889	* 70
1932 - 1	4.0		340	\$10	1-03	312	900	8 8	8	3	- R-E	199	210.
1.645 - 3	. ~		1351	•013	7-67	.313	-003	3	000	000	2.72 -3	1991	410-
1,408 - 3	خ ا		.353	110.	6-24 -4	.313	•003	•	000	900.	2-27 -3	199-	•10 •
1.209 - .356 .008 4.28 - .314 .002 0.0. .000 .000 .138 - .571 .007 .251 .007 .251 .007 .251 .007 .251 .007 .251 .007 .000 .000 .138 - .571 .007 .258 - .258 .208 .251 .208 .20	r		*354	600.	5.25 -4	•314	700*	•	000	000	1.93 -3	699.	110.
1.025 - 3 557	٥		.356	800-	1 85.4	.314	7005	ð,	200.	800	F- 99-7	129.	c10.
1.55 1.55	•	1.029 -3	.357	200-	7.51	-315	100.	.	300	9 8		270.	900
6.567 4 359 .000 1.21 4 316 .001 0	ac r	8.8UV	5000	9	20.7	-512	100	.	35	3 5		,	000
5.547 + .360 .003	, -	7 7 7 7	250	600	4000	91E	100	.	900	900	1	675	500-
4,762 -4 360 .003 9,25 -5 .316 .000		5-547 -4	360	400	1771	316	000	3	000	000	1 2:0	.670	
4.065 -4 .361 .003 7.09 -5 .316 .300 .000 .000 4.02 -4 .678 2.543 -4 .361 .002 .316 .000 .000 .000 4.02 -4 .678 2.549 -4 .361 .002 2.44 -5 .316 .000 .000 2.49 -4 .679 2.549 -4 .362 .002 2.44 -5 .316 .000 0.00 2.49 -4 .679 1.885 -4 .362 .001 1.487 -5 .316 .000 0.00 2.49 -4 .679 1.885 -4 .362 .001 1.487 -5 .316 .000 0.00 2.49 -4 .679 1.885 -4 .362 .001 1.487 -5 .316 .000 0.00 2.49 -4 .679 1.604 -4 .362 .001 1.10 -5 .316 .000 0.00 1.217 -4 .679 1.604 -4 .362 .001 1.510 -5 .316 .000 0.00 1.30 1.217 -4 .679 1.214 -4 .363 .001 4.525 -6 .31	, ₍₁)	4-762 -4	360	100	9-25 -5	.316	000	÷	000	000*	5.69 14	.677	100.
3.473 -4 361 .002 5.43 -5 .316 .000 0000 .000 4.02 -4 .678 2.573 -4 .361 .002 3.19 -5 .316 .000 0000 .000 2.37 -4 .678 2.573 -4 .362 .002 2.44 -5 .316 .000 0000 .000 2.37 -4 .678 2.190 -4 .362 .002 2.44 -5 .316 .000 0000 .000 2.43 -4 .679 1.685 -4 .362 .001 1.81 -5 .316 .000 0000 .000 2.43 -4 .679 1.605 -4 .362 .001 1.10 -5 .316 .000 0000 .000 1.51 -4 .679 1.605 -4 .362 .001 1.10 -5 .316 .000 0000 .000 1.51 -4 .679 1.605 -4 .363 .001 6.43 -6 .316 .000 0000 0000 1.30 -4 .679 1.605 -5 .363 .001 4.92 -6 .316 .000 0000 0000 0000 6.24 -5 .680 6.917 -5 .363 .001 2.89 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 2.36 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.917 -5 .363 .000 1.70 -6 .316 .000 0000 0000 0000 6.24 -5 .680	, pri	4-065 -4	.361	.003	7.09 -5	.316	000	ŏ	900	000	† F.	.677	.00.
2.549 -4 .361 .002 3.19 -5 .316 .000 0000 2.00 2.37 -4 .678 2.1940 -4 .362 .002 2.44 -5 .316 .000 0000 0000 2.49 -4 .678 2.1940 -4 .362 .002 2.44 -5 .316 .000 0000 0000 2.49 -4 .679 1.885 -4 .362 .001 1.87 -5 .316 .000 0000 2.07 -4 .679 1.625 -4 .362 .001 1.45 -5 .316 .000 0000 2.07 -4 .679 1.224 -4 .362 .001 1.45 -5 .316 .000 0000 1.37 -4 .679 1.225 -5 .363 .001 6.43 -6 .316 .000 0000 1.12 -4 .680 2.129 -5 .363 .001 6.43 -6 .316 .000 0000 0000 1.12 -4 .680 2.227 -5 .363 .000 2.22 -6 .316 .000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.30 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.30 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 2.257 -5 .363 .000 1.70 -6 .316 .000 0000 0000 0000 6.24 -5 .680		3.473 -4	196.	-005	5.43 -5	.316	000	•	000	000	1-07-	5.4	00
2.1547 -4 .362 .002 2.44 -5 .316 .000 0000 .000 2.43 -4 .6779 1.885 -4 .362 .001 1.87 -5 .316 .000 0000 .000 2.07 -4 .6779 1.885 -4 .362 .001 1.87 -5 .316 .000 0000 0000 1.77 -4 .6779 1.625 -4 .362 .001 1.87 -5 .316 .000 0000 0000 1.21 -4 .6779 1.224 -4 .363 .001 6.43 -6 .316 .000 0000 0000 1.30 -4 .6779 1.225 -5 .363 .001 2.89 -6 .316 .000 0000 0000 1.22 -6 .680 6.027 -5 .363 .000 2.22 -6 .316 .000 0000 0000 1.22 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.027 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680	· ·	2.973 -4	.361	700-	4-16 -5	-316	000-	.	200	300		2	2 5
1.625 -4 .362 .001 1.87 -5 .316 .000 0000 .000 2.07 -4 .679 1.625 -4 .362 .001 1.87 -5 .316 .000 0000 .000 1.37 -4 .679 1.625 -4 .362 .001 1.87 -5 .316 .000 0000 1.37 -4 .679 1.625 -4 .363 .001 6.43 -6 .316 .000 0000 1.30 -4 .679 1.625 -4 .363 .001 6.43 -6 .316 .000 0000 1.30 -4 .680 1.625 -5 .363 .001 6.42 -6 .316 .000 0000 1.30 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 1.625 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680	•	2.549 -4	296.	700	5-19-5 5-44-6	•310	3	.		36	1 29-7	2	
1.404 -4 .362 .001 1.43 -5 .316 .000 0000 1.51 -4 .679 1.404 -4 .362 .001 1.10 -5 .316 .000 0000 1.51 -4 .679 1.404 -4 .362 .001 1.10 -5 .316 .000 0000 1.30 .451 -4 .679 1.404 -4 .363 .001 6.43 -6 .316 .000 0000 1.30 .400 1.30 .400 9.129 -5 .363 .001 6.43 -6 .316 .000 0000 1.00 1.31 -5 .680 6.907 -5 .363 .001 2.22 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 6.007 -7 .207		1.885 -4	44.2	100	1.87	416	900	å	000	000	7 60-7	67.9	100
1.404 -4 .362 .001 1.504 -6 .316 .000 0.0 .000 1.51 -4 .679 1.214 -4 .363 .001 1.510 -5 .316 .000 0.0 .000 1.30 -4 .679 1.052 -4 .363 .001 6.43 -6 .316 .000 0.0 .000 1.12 -4 .680 9.129 -5 .363 .001 6.43 -6 .316 .000 0.0 0.00 9.62 -5 .680 7.925 -7 .363 .001 2.89 -6 .316 .000 0.0 0.0 0.0 9.62 -5 .680 6.027 -5 .363 .001 2.22 -6 .316 .000 0.0 <td></td> <td>1-675 -4</td> <td>3</td> <td>100</td> <td>1-44-5</td> <td>316</td> <td>000</td> <td>3</td> <td>700</td> <td>000</td> <td>1</td> <td>200</td> <td>100.</td>		1-675 -4	3	100	1-44-5	316	000	3	700	000	1	200	100.
1.214 -4 .363 .001 8.41 -6 .316 .000 0000 1.30 -4 .679 1.052 -4 .363 .001 6.43 -6 .316 .000 0000 0000 1.12 -4 .680 9.129 -5 .363 .001 3.77 -6 .316 .000 0000 9.00 9.00 9.00 9.00 9.00	٠.	1-404-1	.362	100	S- 01-1	-316	900	ဝံ	000	30.	1-51 -4	.679	100-
1.052 -4 .363 .001 6.43 -6 .316 .000 0000 .000 1.12 -4 .680 9.129 -5 .363 .001 4.92 -6 .316 .000 0000 9.62 -5 .680 7.925 -5 .363 .001 2.89 -6 .316 .000 0000 8.31 -5 .680 6.921 -5 .363 .000 2.22 -6 .316 .000 0000 6.24 -5 .680 5.257 -5 .363 .000 1.70 -6 .316 .000 0000 6.24 -5 .680 4.625 -5 .363 .000 1.30 -6 .316 .000 0000 4.76 -5 .680 6.000 .000 4.76 -5 .680 6.000 6.000 6.000 6.000 6.76 -5 .680 6.000 .000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.76 -5 .680 6.000 .000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.76 -5 .680 6.000 6.000 6.000 6.76 -5 .680 6.000			.363	100.	8.41 -6	.316	000-	•	000	000	1.30	.679	100-
9.129 -5 .363 .001 4.92 -6 .316 .000 0000 9.62 -5 .680 7.925 -7 .363 .001 3.77 -6 .316 .000 0000 0000 8.31 -5 .680 6.001 2.28 -6 .316 .000 0000 0000 6.24 -5 .680 6.021 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.25 -5 .363 .000 1.70 -6 .316 .000 0000 0000 6.24 -5 .680 6.000 6.000 6.00 6.24 -5 .680 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.000 6.24 -5 .680 6.000 6.000 6.000 6.000 6.24 -5 .680 6.0000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.	~	•	.363	100.	6-43 -6	.316	•000	•	000	000	1-12 +	9.	100.
7.525 -5 .343 .001 3.77 -6 .316 .000 0000 .000 8.31 -5 .480 6000 0000 8.31 -5 .480 6000 0000 8.31 -5 .480 6000 0000 77.20 -5 .480 6000 6.24 -5 .480 6000 0000 6.24 -5 .480 6000 1.70 -6 .316 .000 0000 6.00 6.00 5.43 -5 .480 6000 1.70 -6 .316 .000 0000 6.00 6.00 6.00 6.00 6.00	~	١	.363	100-	9- 76.4	976.	000	•	200	000	3.6	999	100-
6.907 -5 .363 .001 .2.87 -6 .316 .000 0000 6.24 -5 .680 6.000 6.24 -5 .680 6.000 0000 6.24 -5 .680 6.000 6.27 -5 .363 .000 1.70 -6 .316 .000 0000 0000 5.43 -5 .680 6.000 6.25 -5 .363 .000 1.30 -6 .316 .000 0000 0000 6.16 -5 .680 6.000			.363	100°	3-77 -6	-316	9	ċ	3	38	8-31 -5	2	รู้รั
6.021 =5 .363 .000 2.22 =6 .316 .000 0000 .000 6.24 =5 .080			.363	100-	2-89 -0	-310	000	.		3	C- 07:	200	100
5-257 -5 .363 .000 1.70 -6 .316 .000 U000 .000 .000 .000 .000 .000	ø		.363	999	7-77	.316	000	.	000	990	6-24-5	089-	000
4.625 = 5 .363 .000 1.30 = 6 .316 .000 0000 .000 4.18 = 5 .660 + 0.00	~	257	.363	000	1-70 -6	.316	000	.	000	900	0.43 	200	3
1884 - 1965 - 19	6 0	2	.363	000	9- 06-1	916	000	;	3	33	C 0 0 1	200	3
	.	9	.363	000	1- 66-6	076	3	š	3	3	6 01.		

	Ajt.	Rayleigh	Rayleigh	Rayleigh	Aerosol	Aerosol	Acrosol	Ozone	Ozone	Ozome	ii.	Ert	Ext.
Column		atten.	optical	optical	atten.	optical	optical	absorp.	optical	optical	coeff.	optical	optical
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1,500 - 2	•	2-644 -2	000	. 223	1-80 -1	000	-285	1.25 -5	000	100.	2.06 -1	99.	-509
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		2-400	-025	861	7-92 -2	061.	.155	2- +1-1	000.	100	1-63-1	.155	.355
1,555 - 2	. 2	2-173 -2	940	-175	3-45 -2	201-	960	1-03 -5	. 000	100.	5- 65-5	¥27	-275
1,550	Ę	1-963 -2	690.	.155	7- #:1	.211	+10-	8.75 4	000	100	3-40 -2	-279	.230
1,450	•	1-769 -2	-087	.136	7.59 -3	.222	.063	7.91 -6	000	100	2-53 -2	-309	102.
1,2,74	ر.	1.5902	507	611.	5-72 -3	.228	•026	7.73 4	-000	100	7- 91-7	35	117.
1,2,14	•	1-4252	-119	104	4.03 -3	-233	-052	4.50	000	100	7- 69-1	765	167-
1,135	~	1-274 -2	.133	160.	3.75 -3	-237	3	08*2	200	00.	7- 8-1	25	7
	∞ :	1-135 -2	-145	-010	3.86 -3	.241	440	9 86 1	000	100	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	9 5	901
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	o	1-008	-155	999	3.70 -3	-242	9	9-63	900	100	7- 8-1	3	107
	2		-165	.059	3-61 -3	-248	•036	C- 27-1	900	100	7- 0-1	77	960
\$\begin{array}{c c c c c c c c c c c c c c c c c c c	-		.173	-020	3.38 -3	-252	•033	1-61 -5	000	700	7- 11-1	0	
5.575 - 3 1.57	71	6-733 -3	- 1 80	.043	3.55 -3	-255	-059	2.17 -5	000	700	7- 60-1		*
4,515 -1,57 -1,52 -2,52 -2,52 -0,23 -1,54 -0,000 -0,001	13	5.755 -3	.187	.037	3.28 -3	-259	-056	5-96-2	000	700	6- 10-6		100
1,201 1, 100 1,	<u>*</u>	¢- 916 • 4	.192	. Û.	3.21 -3	.262	•053	3-35 -5	000	700	5- 91 · E	***	^ ·
3,093 3,209 4,209 4,000 <td< td=""><td>12</td><td>4-204 -3</td><td>.197</td><td>.027</td><td>3-02 -3</td><td>.205</td><td>•070</td><td>3.46 -5</td><td>000</td><td>6</td><td>- A-L</td><td>79.</td><td>\$</td></td<>	12	4-204 -3	.197	.027	3-02 -3	.205	•070	3.46 -5	000	6	- A-L	79.	\$
1,002 -2.04 -2.05 -2.04 -0.00 -0.01 -5.04 -0.00 -0.01 -5.04 -2.05 -0.00 -0.01 -5.04 -2.05 -0.00 -0.01 <td< td=""><td>91</td><td>3-593 -3</td><td>•200</td><td>•023</td><td>2-87 -3</td><td>. 268</td><td>-017</td><td>3-60 -5</td><td>000</td><td>700</td><td>6-50-3</td><td></td><td>5</td></td<>	91	3-593 -3	•200	•023	2-87 -3	. 268	-017	3-60 -5	000	7 00	6-50-3		5
2.256 ± 3. 207 . 0.11	11	3-072 -3	•50	070	2-84 -3	.271	*10 *	3.88 -5	8.	700	2.8.2	.473	100
2.255 - 3 2.29 0.10 0.21 -2.75 -0.00 -0.01 <t< td=""><td>87</td><td>2-626 -3</td><td>-207</td><td>110-</td><td>2-75 -3</td><td>.274</td><td>110-</td><td>4-27 -5</td><td>000</td><td>100</td><td>5-41 -3</td><td>•</td><td>•050</td></t<>	87	2-626 -3	-207	110-	2-75 -3	.274	110-	4-27 -5	000	100	5-41 -3	•	•050
1.645 = 1.21	6	2.265 -3	.209	\$10°	2.31 -3	.276	8	4-975	. 000	100*	4-61 -3	*	† 70.
1,644 - 1	50	1-919 -3	*211	-012	1-70 -3	.276	-00	5.75 -5	000	100	3.67 -3	064.	-020
1.187 - 3	21	1-634 -3	.213	•010	1-23 -3	-280	-005	7 33	000	100-	2-93 -3	.493	•10-
1.187 - 3 . 216	22	1.393 -3	.214	600	9-26 -4	-281	90.	6-69 -5	100	100-	2-39 -3	.496	*10 *
1-013 - 3	23	1-187 -3	-216	900-	7-00-4	.28ì	•	6-93 -5	100	100	1.97 -3	164.	-011
8.652 +	5 *	1.013 -3	.217	100	5-62 -4	-282		•	100.	900	F- \$-1	85	010
5.356 - 4 2.23 .005 \$7.570 - 5 .001 .000 \$7.570 - 5 .001 .000 \$7.570 - 5 .001 .000 \$7.570 - 5 .001 .000 \$9.571 - 5 .001 .000 \$9.571 - 5 .001 .000 \$9.771 -	25	8-652 -4	.218	•00•	4°73 4	- 783		•	100	8	1.40 -3	700.	
5.434 + .219 .004	56	7-394 -	-219	-005	+ 71-4	-283		•	700	300	f- 12-1	ų.	
5,413 +	27	6.324-4	-513	• 00•	3-16 -4	-283	8	4.93	100	8	4°6	\$.	
4,634, 4 .220 .003 1.86 4 .001 3.74 -5 .001 .000 6.31 -5 .001 .000 6.01 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 4.77 -4 .001 .000 1.70 -5 .001 .000 2.78 -5 .001 .000 2.79 -5 .001 .000 2.79 -5 .001 .000 2.79 -5 .001 .000 2.79 -5 .001 .000 2.79 -5 .001 .000 2.79 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 .001 .000 1.70 -5 <td< td=""><td>88</td><td>2.413 +</td><td>.220</td><td>100.</td><td>2-42 +</td><td>-284</td><td>700</td><td>4-30 -2</td><td>100</td><td></td><td>9.0</td><td>606</td><td>3</td></td<>	88	2.413 +	.220	100.	2-42 +	-284	700	4-30 -2	100		9.0	606	3
3.874 + .221 .003	29	4-636 -4	-220	-003	1-86 4	-284	100	3.74 -5	100	9	*	ŝ	100
2,409 + 221 .002 1.09 + 278 2.76 + 000 2.76 + 000 2.77 + 000 </td <td>20</td> <td>3.874 .4</td> <td>.221</td> <td>.003</td> <td>1-42 +</td> <td>-284</td> <td>3</td> <td>3.16 -5</td> <td>100</td> <td>8</td> <td>1:0</td> <td>9</td> <td>500</td>	20	3.874 .4	.221	.003	1-42 +	-284	3	3.16 -5	100	8	1:0	9	500
2.926 + .221 .002	1 6	4.400	.221	- 002	1-00-1	-284	900	C- 22-7	100	3			
2.134 -4	7	7.926 -	127	200-	6-33	197-	9	(·)	3	3	3 %		è
1.137 -4 222 .001 3.75 -5 .284 .000 1.51 -5 .001 .001 .001 .235 -4 .000 1.26 -5 .001 .001 .001 .001 .001 1.58 -4 .225 .001 .001 .001 1.067 -4 .235 .001 .000 1.067 -5 .236 .000 1.066 -5 .001 .000 1.067 -6 .001 1.000 1.067 -4 .235 .000 1.067 -6 .001 1.000 1.067 -4 .235 .000 1.067 -6 .001 1.000 1.067 -4 .235 .000 1.067 -6 .001 1.000 1.0	.	2.499 -4	777	200-	6- 96-0	197-	900	5:	3				
1.156 -4 .222 .001	\$;	1 47.7	777.	705	0 49 ¢	107.	3		100	3		3	100
1.345 -4 .222 .001	5 4	179-1	777		0 · (v)	1070	36	1.24			1	905	700
1.156 -4 .223 .001 1.69 -5 .284 .000 6.85 -6 .001 .000 1.542 -4 .223 .001 1.69 -5 .284 .000 6.85 -6 .001 .000 1.20 -4 .223 .001 1.29 -5 .284 .000 6.85 -6 .001 .000 1.00 1.00 1.00 1.00 1.00 1.0	2 6	1-366	222	5	2.29	284	000	1-06-1	100	000	1-67	2000	100-
9.987 -5 .223 .001 1.29 -5 .284 .000 7.59 -6 .001 .000 1.20 -4 .7 .5 .6 .6 .001 .000 1.20 -4 .7 .5 .6 .6 .2 .001 .000 1.20 -4 .7 .5 .6 .6 .2 .001 .000 1.20 -4 .7 .5 .6 .6 .001 .000 1.20 .4 .7 .5 .2 .2 .001 .000 5.79 -6 .285 .000 4.16 -6 .001 .000 1.46 -5 .2 .2 .000 5.79 -6 .285 .000 2.6 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2 .5 .5 .0 .0 .2 .2 .2 .0 .0 .2 .2 .2 .0 .0 .2 .2 .2 .0 .0 .2 .2 .2 .0 .0 .2 .2 .2 .0 .0 .2 .2 .2 .2 .0 .0 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2	. 5	1.158 -4	2.23	100	1.60	-284	000	8.85	100	900	1.42	.503	.001
6.625 -5 .223 .001 9.87 -6 .285 .000 6.51 -6 .001 .000 1.03 -4 7.461 -5 .223 .001 7.56 -6 .285 .000 4.16 -6 .001 .000 7.46 -5 6.464 -5 .223 .000 5.79 -6 .285 .000 4.16 -6 .001 .000 7.46 -5 5.410 -5 .223 .000 3.39 -6 .285 .000 2.60 -6 .001 .000 6.34 -5 4.244 -5 .223 .000 2.60 -6 .285 .000 2.02 -6 .001 .000 4.71 -5 3.700 -5 .223 .000 1.59 -6 .285 .000 1.26 -6 .001 .000 4.06 -5 2.42 -5 .223 .000 1.53 -6 .000 1.26 -6 .001 .000 4.06 -5 2.510 -5 .223 .000 1.51 -6 .000 1.00 2.00 2.00 2.510 -5 .223 .000 6.95 -7 <td>2</td> <td>9-987 -5</td> <td>.223</td> <td>100</td> <td>1.29 -5</td> <td>-284</td> <td>000</td> <td>7-59 -</td> <td>100</td> <td>000</td> <td>1.20</td> <td>-509</td> <td>100</td>	2	9-987 -5	.223	100	1.29 -5	-284	000	7-59 -	100	000	1.20	-509	100
7.461 -5 .223 .001 7.56 -6 .285 .000 5.32 -6 .001 .000 7.46 -5 .002 6.46 -5 .223 .000 5.79 -6 .285 .000 3.25 -6 .001 .000 7.46 -5 .000 6.46 -5 .223 .000 5.79 -6 .285 .000 2.60 -6 .001 .000 6.30 -5 .000 6.30 5.40 -5 .223 .000 1.99 -6 .285 .000 1.56 -6 .001 .000 6.471 -5 .223 .000 1.99 -6 .285 .000 1.56 -6 .001 .000 6.471 -5 .223 .000 1.83 -6 .285 .000 1.56 -6 .001 .000 3.51 -5 .223 .000 1.87 -6 .285 .000 1.86 -7 .001 .000 3.51 -5 .223 .000 6.95 -7 .285 .000 6.51 -7 .001 .000 2.60 -5 .223 .000 6.95 -7 .285 .000 6.51 -7 .001 .000 2.60 -5 .225 .223 .000 6.96 -7 .285 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 2.60 -5 .000 6.51 -7 .001 .000 6.51 -7 .001 .000 6.51 -7 .0	3	8-625 -5	•223	100	9-87 -6	-285	000-	6-51 6	180.	30.	1.63	503	100-
6.464 -5 .223 .000 5.79 -6 .285 .000 4.16 -6 .001 .000 7.46 -5 .285 .285 .285 .285 .285 .285 .285 .28	3	7-461 -5	-223	100	7-56 -6	-285	000-	5.32 -6	- 001	000	5- 52-5	200	-001
5.610 -5 .223 .000	23	6-464 -5	.223	900	5-79 -6	-285	000	₹-16 £	18.	80.	- # ·	805	100
4.876 -5 .223 .000 3.39 -6 .285 .000 2.60 -6 .001 .000 5.46 -3 4.244 -5 .223 .000 2.56 -6 .285 .000 1.56 -6 .001 .000 4.71 -5 3.700 -5 .223 .000 1.59 -6 .285 .000 1.24 -6 .001 .000 4.06 -5 2.842 -5 .223 .000 1.51 -6 .285 .000 9.76 -7 .001 .000 3.51 -5 2.510 -5 .223 .000 6.95 -7 .285 .000 7.80 -7 .001 .000 2.46 -5 2.217 -5 .223 .000 6.95 -7 .285 .000 6.51 -7 .001 .000 2.46 -5	£		-273	000	4-43 -6	-285	000	3.25 -6	100	900	S- #:-9	605.	900
4.244 -5 .223 .000 2.60 -6 .285 .000 2.02 -6 .001 .000 4.04 -5 .233 .000 1.99 -6 .285 .000 1.56 -6 .001 .000 4.06 -5 .233 .000 1.53 -6 .285 .000 1.24 -6 .001 .000 3.51 -5 .223 .000 1.57 -6 .285 .000 9.76 -7 .001 .000 3.56 -5 .225 .000 0.95 -7 .285 .000 7.80 -7 .001 .000 2.46 -5 .225 .000 6.95 -7 .285 .000 7.80 -7 .001 .000 2.46 -5 .225 .000 6.86 -7 .285 .000 6.51 -7 .001 .000 2.56 -5 .225 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.000 7.80 -7 .000 0.0000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	\$		•223	900.	3-39 -6	-285	9	5-60 -6	3	80	7. 3. ·	5	000
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3.230 -5 .223 .000 1.53 -6 .285 .000 1.24 -6 .001 .000 3.51 -5 . 2.842 -5 .223 .000 1.17 -6 .285 .000 7.40 -7 .001 .000 3.06 -5 . 2.510 -5 .223 .000 6.95 -7 .285 .000 6.51 -7 .001 .000 2.00 -5 . 2.217 -5 .223 .000 6.66 -7 .285 .000 6.51 -7 .001 .000 2.35 -5 .	9	3-700 -5	.223	000	1-99 -6	-285	000	7·20 P	8.	80.	4.8.	600	000
2.842 -5 .223 .000 1.17 -6 .285 .000 9.76 -7 .001 .000 3.08 -5 . 2.510 -5 .223 .000 6.95 -7 .285 .000 7.80 -7 .001 .000 2.66 -5 . 2.217 -5 .223 .000 6.86 -7 .285 .000 6.51 -7 .001 .000 2.35 -5 .	†	3-230 -5	•223	000	1-53 -6	-285	9	1.24 -6	100	000	C- 16-6	200	
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- (- CC+7 TAN 1- 1- 1C+9 DOM: <827)- 99*9 DOM: <77* <-	.	c- 01c-7	677-	900	-	687		200	3 3	3	3 7 7	8	gna
	8	2-211 -5	.223	000	•	- 785		/- TC-0	100		C- CC-7		

Table 4. 10 Parameters at 0, 50 microns

			•		•.		•	i¢ ′				
:	4:50	4114	di-fi-d		V V	Amond	8	Garac	Ozone	Est	Ext	Ed
į	etten	on the same	ontice!	atter	centical	omtical		ootical	ortical		optical	ortical
	coeff.	thick.	thick.	coeff.	thick.	thick	coeff.	thick	Chick		thick	tt ick.
Î	(km ⁻¹)	(Q-P)	(- -	(Fm -1)	(q-p)	€-4	(km ⁻¹)	(Q - Ir)	€ €		(Q - P)	\$ = =
д	ø,	6 .44	, _L u	<i>6</i>	r _æ		ß ₃	13	13,	bent ent	ext	, ext
		2	941	1-53-1	000	744	1 22	000	- 0 <u>-</u>	10 40 1	000	: 104
> ~	1-557 -2	910	671	7.35 -2	120	*	1.12	200	710-	8-91	137	.284
. ~	1-410 -2	.031	\$11 *	3-17 -2	.173	160	1-10-1	000	110.	4-59 -2	*50	717
· ^	1.273 -2	.045	.100	1-33 -2	-195	690 *	8-63 -5	000	110.	2-19-2	047-	181
*	1-148 -2	.057	.088	7.04 -5	-206	-058	7-80 -5	000	70.	1.86 -2	-263	158
.		990	-077	5-31	-212	-052	7-62 -5	000	10.	7- 25-1	25.	147
•	9-245 -3	-01	990	3-74-3	912-	3	C- C+-1	100	110	7- W-1	447	
~	8-263 -3	980	.050	3.48	-220	į	7-69-5	100	170	2- 81-1	-307	-114
æ	7-364 -3	1	150.	5-58-5	577	5		100	110	77	27.	500
٠ :	6-541 -5	101-		30.44	976	1037				7 7 7	13C+	260
2 :	5 50 5	21.0	200	1-14-2	217		1 3 1	3		17.4	7	420
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1 5		27	470	3.04 -3	240	426	2.92	100	070	7.07	36.3	880
2 2			0.0	2.98 -3	243	120	3-30	700	010	6- 50 -3	369	150.
) -		20	617	2.80 -4	246	10	1	200	010	5-67	376	10.5
7	2. 121 -5	971		7- 99-7	769	510	7 55 4	007	800	- 19. · S	381	o
		22.	210	2-62-2	26.1	210	1	100	000	5. B	384	46
		*	110-	2,55 -3	256	010	1	60	00	4-67-3	.391	030
2 2		**	600	2-15 -3	256	800	1	400	9	4-69-4	.396	.025
		137	500	1.57 -3	258	900	5.66	400	100	3-30 -3	399	.021
7.7	1-060 -3	.138	-001	1-14	-259	500	+ SE +	• 005	100	2.64 -3	104	610
22	9.035 -4	667.	900-	8.59 -4	-260	400-	1 08.9	• 005	900•	2.4 -3		910.
23	7.703 -4	041.	-005	6.57 4	797	•003	1 E1-9	900•	-005	2.11 -3	407	. 013
*	6.574 -4	141.	+00+	₹- 12°5	-262	-005	1 99.9	-00	80.	- ¥:	5	110.
52	5-614 -4	141.	•00•	4-39 -4	-262	-005	6-21 -4	-00-	800	1.62 -3	.411	010
97	+- 196 -+	.142	•003	3.83	-263	100	2.62	900	\$0.	7:	£14.	800.
27	4-103 -4	142	£00°	2-93 -4	-263	100	11			1.19	*1**	3
9 5	1 270.6	647	700	4 67.	242			38	30		414	900
,	2,578 -6	143	700	1-32	797	000	3-12	010	3	1	417	500
3 2	2,212 -4	.143	100-	10-1	-254	900	2.74	010-	700-	7 8.5	-417	.003
35	1.898 -4	\$7.	100.	7.73 -5	-264	000•	2.35 -4	010.	100-	2.6	. 61B	.003
33	1- 129-1	\$1.	100	5-92 -5	-264	000	7-07-	110-	100-	† 77·4	-418	.002
¥.	1-385 -4	‡ :	100	6.53 -5	197-	000	1 20-1	110	100	1	674.	700.
52	1-185 -4	¥.	100	F 20 1	+02-		*	110	700	3:5	À .	700
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, e	7.516	**	100	5- 45-1	792			10	90	7	95	100
9 9		*	000	1-19 -5	-264	000	7-69-7	-011	90	1:2:	8	.001
9		145	000	9-15-6	.264	000	6-42 -5	-011	30.	1 87-1	84.	.00
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74		•145	000	5.37 -6	-264	000	\$- II-	-015	000	\$ - 1: - 0:	•420	.000
4 3	3-640 -5	-145	000	4-11-4	-264	00	3-21 -5	-012	000	7.26 -5	24.	200,
‡		•145	000	3-15 -6	-264	000	2.57 -5	710	900	8	-420	000-
42		•145	000	9- 14-7	197-	200	7-86	710-	3	C- K:	174-	300
\$	2-401 -5	-145	3	1-85 -6	*97		1.54 -5	-015	800	4.12 -5	174-	000
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			110	1.58 -1 .000 5.95 -2 .116 3.00 -2 .116 3.00 -2 .116 5.05 -3 .116 5.05 -3 .116 5.05 -3 .116 5.05 -3 .206 3.25 -3 .206 3.25 -3 .206 3.25 -3 .206 2.05 -3 .211 2.05 -3 .221 2.05 -3 .221 2.05 -3 .221 2.05 -3 .221 2.05 -3 .221 2.05 -4 .224 5.05 -4 .246 6.15 -4 .246 6.15 -4 .246 7.17 -4 .246
136 23 24 24 24 24 24 24 24 24 24 24 24 24 24				6.95 -2 .114 13.00 -2 .116 13.00 -2 .116 6.66 -4 .194 5.02 -4 .196 3.57 -4 .208 3.57 -4 .208 3.55 -4 .208 3.17 -4 .208 2.55 -4 .227 2.55 -4 .227 2.55 -4 .227 2.65 -4 .227 2.65 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 6.27 -4 .246
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**************************************				5-02 -3 .200 3-25 -3 .200 3-25 -3 .200 3-25 -3 .205 3-25 -3 .205 3-12 -3 .218 3-12 -3 .218 2-36 -3 .221 2-36 -3 .221 2-36 -3 .235 2-3 .240 2-36 -3 .240 2-36 -4 .240 2-36 -4 .240 2-36 -4 .240 2-36 -4 .240 2-37 -4 .240 2-37 -4 .240 2-37 -4 .240 2-37 -4 .240
945 935 935 935 935 935 935 935 935 935 93	**********			2.55 - 3 - 205 3.25 - 3 - 205 3.17 - 3 - 205 3.17 - 3 - 205 3.18 - 3 - 205 2.55 - 3 - 221 2.55 - 3 - 221 2.55 - 3 - 221 2.55 - 3 - 221 2.55 - 3 - 221 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 3 - 224 2.55 - 4 - 224 2.57 - 4 - 224 2.77 - 4 - 224 2.77 - 4 - 224 2.77 - 4 - 224 2.77 - 4 - 224 2.77 - 4 - 224 2.77 - 224
74.5 23.38 8.5 22.5 6.5 22.5 6.5 20.5 20.5 20.5 20.5 20.5 20.5 20.5 20	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			3.29 -3 .208 3.29 -3 .208 3.25 -3 .208 3.17 -3 .211 2.26 -3 .221 2.88 -3 .221 2.86 -3 .224 2.87 -4 .246 1.08 -3 .246 1.08 -3 .246 1.08 -4 .246 6.22 -4 .246 6.22 -4 .246 6.22 -4 .246 7.93 -4 .246 7.93 -4 .246 7.93 -4 .246 7.93 -4 .246 7.93 -4 .246
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222 2226 2226 2326 2326 2326 2326 2326				2.975 2.885 2.885 2.885 2.825 2.845 2.85 2.495 2.40 2.495 2.45 4.156 2.49 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.40
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223 220 2117 2117 200 200 200 200 200 200 200 200 200 20		·		2.88 -5 -227 2.655 -5 -239 2.655 -5 -239 2.657 -5 -239 2.657 -5 -239 2.657 -5 -239 2.657 -5 -240 2.657 -5 -240 2.657 -5 -240 2.657 -5 -240 2.77 -5 -240 2.77 -5 -240
22 22 22 22 22 22 22 22 22 22 22 22 22				2.62235 2.55233 2.55233 2.49238 2.49246 1.49246 6.22246 6.22246 6.22246 7.93246 7.93246 7.93246 7.93246 7.93246
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1110 1110 1110 1110 1110 1110 1110 111				2.52 2.38 2.49 2.38 2.03 2.38 2.03 2.40 1.49 2.46 6.22 2.46 6.22 2.46 6.25 2.46 2.77 2.48
2005 2006 2006 2006 2006 2006 2006 2006	,,,,,,,,,,,		77777777777	2.49 -3 -238 2.41 -3 -240 2.41 -3 -240 2.41 -3 -240 1.49 -3 -245 6.22 -4 -247 4.15 -4 -248 3.65 -4 -248 2.17 -4 -248
200 200 200 200 200 200 200 200 200 200	*******			2.41 -3 -240 2.03 -3 -2 -240 1.49 -3 -245 1.49 -3 -245 6.22 -4 -246 4.93 -4 -248 5.52 -4 -248 2.77 -4 -248
2003 2003 2003 2003 2003 2003 2003 2003	•			2.03 -5 -242 1.49 -5 -244 6.22 -4 -246 6.22 -4 -246 6.25 -4 -246 7.55 -4 -248 3.65 -4 -248 2.77 -4 -248
	1999999			1.49 -3 -245 1.08 -3 -245 1.08 -3 -245 6.22 -4 -246 4.15 -4 -248 3.62 -4 -248 2.77 -4 -248
\$5000000000000000000000000000000000000			\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1.08 -3 -245 8.13 -4 -246 6.22 -4 -247 4.93 -4 -248 4.15 -4 -248 3.62 -4 -248 2.77 -4 -249
5000000	1.7 7 7 9			6.22 -+ .245 6.22 -+ .246 6.23 -+ .246 6.25 -+ .248 3.62 -+ .248 2.77 -+ .248
2023			7,74	6.22 247 6.93 248 6.15 248 3.62 248 2.17 248
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100-		642	†	2-12
7		-249	†	1-63 -4
-000		-249	†	1-25 -4
900			-5 .249	9.55 -5 .249
000	•		-5 .249	7-31 -5 -249
900	•		-5 .250	5.60 -5250
000	•		-5 -250	4.29 -5 .250
000	•		-5 -250	3.29 -5 .250
900	•		-5-250	2.52 =5 -250
005	1	1	-5 -250	1-93 -5 -250
900			-5 -250	1-48 -5 -250
90	7		-5	1,13 -5 ,250
9 9			250	8.66 =6 .250
3	3			0000
9	7		-6 .250	6-64 -6 -250
90	7		-6 .250	5.08 -6 .250
000	7		-6 250	3-89 -6
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9	•		067.	067 - 9- 87-7
8	7	٠	9-	1.75 -6 .250
000	•		-6 .250	1-34 -6 -250
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ı				2.55 -5 .249 2.50 -5 .249 2.50 -5 .249 2.29 -5 .250 1.93 -5 .250 1.93 -5 .250 1.93 -5 .250 1.93 -5 .250 2.98 -6 .250 2.98 -6 .250 2.98 -6 .250 1.93 -6 .250

ଲାଗ ⊾ା	<u>.</u> 1
(h - 8)	٠
ext. optical thick. (0 - h)	i Eri
Ext. coeff. (ton ⁻¹) $\theta_{\rm ext}$	1
Ozone optical thick. (h - ∞)	
Ozone optical thick. (6 - h)	•
Ozone absorp. coeff. (km ⁻¹)	?
Acrosol optical thick. (h - ∞) r' p'	4
Aerosol optical thick. (0 - h)	P
Acrosol atten. cocff. (km ⁻¹) β	Ç.
Rayleigh optical thick. $(h-\infty)$	-
Rayleigh optical thick. (0 - h)	٠.
Rayleigh atten. coeff. (km ⁻¹)	۲.
(Rm)	.]

34

Table 4.14 Parameters at 0.70 microns

The continue of the continue	Alt	Rayleigh atten.	Rayleigh optical	Rayleigh optical	Acrosol atten.	Aerosol optical	Aerosol optical	Ozone absorp.	Ozone	Ozone	· Ext.	Ext.	Ect.
The control of the	<u>a</u>	coeff. (km²t)	thick. (0 - h)	thick. (h - se)	ooeff. (km ⁻¹)	(0 - b)	thick.	30eff.	thick (0-h)	thick.	(km ⁻¹)	thick (0-b)	trick.
## 55 ## 54 ## 50	4	β,	r,	, u	هر _ي .	ťΦ	.* . ~	æ.	fu.	.f.	est.	, tx	ext
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	0	4-355 -3	000-	-037	1- 35 -1	000	-213	8-19 -5	000	800.	1- 66-1	8.	.258
### ### ### ### ### ### ### ### ### ##		5-95I -3	400.	.033	5-94	-097	-116	7.50 -5	000	900-	6.# -2	101.	TCT.
1,2,2,4 1,000	7	3.586 -3	800.	-029	7- 95-7	-140	* 20.	0.74 -5	000	900°	7- 68-7	P+	011.
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	m 4	3.240 -3	10.	-026	1-08 -2	-158	950	2-75-5	200		1-41-8 8-66-43	61.	25°
1,137 1,132 1,132 1,133 1,13	f ir	2-676-5	710	770	4-29-4	27	8	5-68-5	200	1 00.	, % - 3%	189	690
1,112 - 1	ۍ.	2.352 -3	020	110.	3.02 -3	175	-039	4-97 -5	200	200	5.43 -3	.195	063
1,487 - 1, 1024	~		270.	-015	2.81 -4	-178	950.	5-11 -5	• 000	100-	4.8	~~	.058
1, 10, 10, 10, 10, 10, 10, 10, 10, 10,	Œ	1.873 -5	•056	.013	2.90 -3	181	•033	5-47-5	200.	200-	4-82 -3	-205	£00.
1,100	o	1-654 -3	•026	110.	2-78 -3	-183	- u30	6-46-5	130	100-	4.51 -3	.410	40.
	3 :	1-673	1707	010.	5-11-7	000	170.	8. U.S.	3		1 1	#177	1 0
\$\begin{array}{c} \text{5.65} \tau \text	= :	6- 005-1 1- 1-1-1-1	670	200	6- 4C-7	101	200	33	100	700	100		0.0
Color	<u> </u>	4- 664-6	160.	900	2-66-5	3	010	35	100	700.	3-61 -3	-426	. 034
5.931 4	1 2	8-113 -4	760.	4005	2-41 -3	961.	-017	2.20	.001	-007	3.4 -3	•226	670.
5.073 1	2	6.939 -4	260.	400.	2-79	641.	-015	4- 67-7	100-	900-	5-19 -3	.233	970.
5.070 ± 0.03	91	5-931 -4	.033	*00°	2-15	.231	.013	2.37	700	800	8-7	957	. 022
4.334 - 0.95 </td <td></td> <td>5-070 -4</td> <td>•034</td> <td>.003</td> <td>2-13 -3</td> <td>-203</td> <td>010-</td> <td>2-55 -4</td> <td>200-</td> <td>800</td> <td>2.89</td> <td>• 239</td> <td>670.</td>		5-070 -4	•034	.003	2-13 -3	-203	010-	2-55 -4	200-	800	2.89	• 239	670.
2.699 +	B :	4-3%	\$ 0.00 5.00 5.00		2.06 -5	507-	200	79.7	700	9 9	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	147.	110
2.673 +	61	5- 702			1-13-3	102-	900	77.55	700	5	20.1	777	; :
1.2279 + 1.035 .001 6.93 + 1.21 .003 4.53 + 1.004 .004 .004 .004 .025 .004 .025 .004 .025 .004 .025 .004 .025 .004 .025 .004 .005 .004 .005 .004 .025 .004 .005 .004 .005 .004 .005 .004 .005 .004 .005 .004 .005	2.5	2.693	56.0	700-	\$ 17°7	7.00	200	1 1 2	50	500	7-79-1	647	010
1,960 + 4	77	£- 66.2.7 7.	.035	100.	6-95 -4	-210	603	4-53	400	\$00.	7 R.1	-250	600
1.672 - 1	23	1.96u -4	.038	100-	5-31 -4	-211	-002	4.55 -4	*00*	50.	1.18	157	. 007
1.44.2	54	U- 719*1	•036	700	4-77-4	-212	-005	+ + +	.00	•00°	1.03 -3	.254	900-
1,12,11	52	1-623 -6	-036	100.	3.55 4	-217	100-	***	500	5003	1 1 2 2 3 4	£55.	, oo
6.555 - 6.05	7¢	177-1	8 6	100.	3,09	717	100	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	200	700	9 5	257	1 1 2 2
7.553 -5 .036 .001 1.39 -4 .213 .001 2.46 -4 .000 .001 3.80 -4 .256 .250 .550 .550 .5 .035 .000 8.16 -5 .213 .000 1.57 -4 .007 .001 3.80 -4 .256 .250 .5 .037 .000 8.16 -5 .213 .000 1.57 -4 .007 .001 2.20 -4 .257 .251 .252 .253 .253 .253 .253 .253 .253 .253		5.935 -5	, d	100	1.81	517	190	2-8-7	900	700	5.53 +	.455	£00.
5.55u -5095000	£ 7	7-553 -5	-036	100-	1-39 -4	.213	100	2.46 4	•000	Too-	4-62 -4	957-	.00
5.627 -5 .035 .000 8.16 -5 .213 .000 1.57 -4 .001 .001 2.23 -4 .257 .000 4.78 -5 .213 .000 1.57 -4 .001 .001 2.23 -4 .257 .000 4.78 -5 .213 .000 1.57 -4 .001 .001 1.58 -4 .257 .000 2.21 -5 .013 .000 1.001	9	2-500 -5	.035	• 000	1-07	-213	000	1 80.7	-00	100	1 3	-256	200.
4.124 -5 .037 .000 4.78 -5 .213 .000 1.37 -4 .007 .001 1.85 -4 .257 .000 2.45 -5 .037 .000 2.45 -5 .213 .000 1.12 -4 .007 .001 1.85 -4 .257 .000 2.45 -5 .013 .000 1.65 -5 .213 .000 8.30 -5 .007 .000 1.08 -4 .257 .000 2.45 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.26 -5 .013 .000 1.27 .000 1.08 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.28 .000 1.38 .0000 1.38 .000 1.38 .000 1.38 .000 1.38 .000 1.38 .000 1.38 .000 1.38 .000 1.38 .000 1.38	∓ ?	5-627 -5	960-	000	8-16-5	-213	9 6	78-1	200	100	7 7 7	25.70	705
3.523 -5 .037 .000 3.67 -5 .213 .000 1.12 -6 .007 .001 1.583 -4 .257 .255 .037 .000 2.215 -5 .213 .000 8.30 -5 .007 .001 1.57 -4 .257 .255 .037 .000 1.265 -5 .213 .000 8.30 -5 .007 .001 1.27 -4 .257 .255 .037 .000 1.265 -5 .213 .000 8.30 -5 .007 .000 1.00 -1.20 -4 .257 .255 .037 .000 1.265 -5 .213 .000 6.95 -5 .008 .000 1.00 -5 .258 .258 1.549 -5 .037 .000 1.265 -5 .213 .000 6.95 -5 .008 .000 1.00 6.44 -5 .258 1.265 .037 .000 6.34 -6 .213 .000 2.74 -5 .008 .000 5.25 -5 .258 1.265 .258 1.267 .250 .250 .255 .258 1.267 .250 .258 1.275 .250 .258 1.275 .250 .258 1.275 .250 .258 1.275 .250 .258 1.275 .250 .258 1.275 .275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258 1.275 .258	7 7		740		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			7 7 7 7	100	000	37	757	177
3-016 -5 .037 .000	3.7		.037	000	3-67 -5	213	200	+ 21-1	. 20	-001	1.63	.457	101
2.555 -5 .037 .000 2.15 -5 .213 .000 8.30 -5 .007 .000 1.30 -4 .257 .222 .237 .000 1.265 -5 .213 .000 6.955 .007 .000 1.00 -4 .256 1.256 1.256 .233 .000 6.955 .008 .000 9.00 9.00 -5 .256 1.256 1.256 .233 .000 6.955 .008 .000 7.40 -5 .258 1.256 1.256 .233 .000 6.955 .008 .000 7.40 -5 .258 1.256 1.255 .258 1.257 .250 .257 .000 7.40 -5 .213 .000 7.40 -5 .008 .000 7.40 -5 .258 1.256 1.257 .250 .257 .250 .257 .257 .257 .257 .257 .257 .257 .257	35		.037	000-	2-31 -5	-213	200	6-16-6	-004	100	1.57 -4	.257	101
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1.232 -5 .037 .000 5.57 -6 .213 .000 2.74 -5 .008 .000 5.29 -5 .258 1.067 -5 .037 .000 4.34 -6 .213 .000 2.74 -5 .003 .000 3.40 -5 .258 1.067 -5 .037 .000 4.34 -6 .213 .000 2.74 -5 .003 .000 3.40 -5 .258 1.067 -5 .037 .000 2.55 -0 .213 .000 1.71 -5 .008 .000 2.22 -5 .258 1.006 -5 .037 .000 1.95 -6 .213 .000 1.32 -5 .008 .000 2.22 -5 .258 1.006 -5 .037 .000 1.50 -5 .213 .000 1.03 -5 .008 .000 1.77 -5 .258 1.007 .000 1.14 -6 .213 .000 6.42 -6 .008 .000 1.46 -5 .258 1.008 .000 1.20 -5 .258 1.009 .000 5.14 -6 .213 .000 5.42 -6 .008 .000 9.44 -6 .258 1.009 .000 5.14 -7 .213 .000 5.48 -6 .008 .000 9.45 -6 .258	, G		740-	eon.	7.50 -6	213	000	4.28 -5	800	200-	\$.\$ •	. 458	700
1.067 -5 .037 .000 4.34 -6 .213 .000 2.74 -5 .000 .000 4.24 -5 .258 3.250 -5 .037 .000 2.55 -6 .213 .000 1.71 -5 .000 .000 2.77 -5 .258 8.064 -5 .037 .000 2.55 -6 .213 .000 1.37 -5 .008 .000 2.22 -5 .258 7.006 -5 .037 .000 1.95 -6 .213 .000 1.35 -5 .008 .000 1.79 -5 .258 6.108 -6 .037 .000 1.14 -6 .213 .000 8.12 -6 .008 .000 1.79 -5 .258 4.451 -6 .037 .000 6.72 -7 .213 .000 6.42 -6 .008 .000 9.44 -6 .258 3.659 -6 .037 .000 5.14 -7 .213 .000 6.42 -6 .008 .000 9.45 -6 .258 3.659 -6 .037 .000 5.14 -7 .213 .000 6.42 -6 .008 .000 9.45 -6 .258	4		.037	000	5-57 -6	-213	020	3-50 -5	800	000.	5-23-5	.258	. Juu
3-2-5 - 0.037 .000 3-52 - 6 .213 .000	75		.037	000.	4-34 -6	-213	000	2-7-5	. O. a	000-	4-24-5	.258	377
8.048 -5 , .037	43		-037	000	3.32 -6	-213	202	2-14-5	900	30	3.5	. 258	070
6.108 -6 .037 .000 1.50 -5 .213 .000 1.03 -5 .008 .000 1.79 -5 .258 .000 1.03 -5 .008 .000 1.79 -5 .258 .000 1.03 -5 .008 .000 1.04 -5 .258 .000 1.04 -5 .058 .000 1.05 .000 1.00 -5 .258 .000 1.00 1.00 -5 .000 1.00 -5 .000 1.00 -5 .000 1.00 -5 .000 1.00 1.00 -5 .000 1.00 1.00 -5 .000 1.00 1.00 1.00 1.00 1.00 1.00 1.0	4 .		-037	000	2.55 -0	.213	000	1.71 -5	200	3	2. 22. 4	957	3
6.108 -5 .037 .000 1.14 -6 .213 .000 84.12 -6 .008 .000 1.46 -5 .258 .258 .258 .258 .258 .258 .258 .25	٥,			200	6.5	617	3	C- 2001	3	3	5 25 7	25.70	
4.691 - 6 .037 .000 8.30 - 7 .213 .000 6.42 - 6 .008 .000 1.20 - 3 .258 .45	0 1		-03/	3	P 4 4	517		R-17-5	6.5	800	5.5	857	200
4.143 -6 .037 .000 6.72 -7 .213 .000 5.13 -6 .008 .000 9.94 -6 .258 3.659 -6 .037 .000 5.14 -7 .213 .000 4.28 -5 .008 .000 8.45 -6 .258	τ 4	4-691-4	7.0	900	R-du -7	213	000	13	800	300	1.20 -5	- 458	000
3.659 -6 .037 .000 5.14 -7 .213 .440 4.28 -5 .008 .000 8.45 -6 .258	. 04	4-143 -6	.037	2000	1- 71-9	-213	000	5-13-6	98	0000	7 3.5	.258	3
	50	3-659 -6	750-	000	5-14 -7	-213	000	4-28	.008	000	8-45	-258	970-

	Rayleigh	Rayleigh	Rayleigh	Acrosol	Acrosol	Acrosol	Ozone	Ozome	Ozone	Ext.	Ext.	Er.
	aften.	optical	optical	atten.	optical	optical	absorp.	optical	optical	coeff.	optical	op ical
ĺ		thick 5	thick.	- Coeff	thick.	thick.	Soeff.	trick Sirk	thick.	. 1	thick:	¥. ∄:
Î		(B-0)	((H-D)	(p-8)	(Em ')	(q-0)	() ()	((Q-P)	§ €
. #	ø,	~ "	` .	er_p.	r _e	.* _C	æ	ħ.	. " w	Z.	, an	rxi ext
9	2-544 -5	000-	170.	1- 17-1	200-	107-	3.50 -5	7000	£00.	1- 06-1	000	977
-	2-309 -3	700-	-113	5-59 -4	160-	607-	3-40 -5	• 000	•003	5-42 -2	460.	-132
~	7-001	. ი პ5	210-	7- 14.7	-131	•069	2.63 -5	200.	thu.	7-79-7	.136	067.
m.	1-633 -3	-007	-015	1.01 -2	-149	750.	2-50 -5	000	£00.	7-07-1	• 155	70
J	L- 702 -3	وي د	.013	5.35 -3	•156	ş	5-97·7	200	£0.	20.7	•165	191.
'n,	1.530 -3	010-	110-	£- +04	191-	90	2-17-2	000	£00.	5-59 -3	171.	. 52
e i	1-3/1-5	110-	010	Z- CP-7	•10+	957	7°10	700	£00.	5- 42-4	2 .	יר אם
~ 0	5- 577-1	510.	700	2.54 -3	101	***	2-62-7	36	500	50.5	3.5	9
0	C 207 5	10.	5.50	7, 7, 7	7.4	100	7 7 7	3	100	71 77	101	7
2	20.00			7.35 -4	175	4		200		1	7	9
2 =	7-577 -4	710-	500-	2.40	178	100	4-60 -5	000	100	4-10-4	57.	16.30
: 2	4-674	200	*0n	2.51 -3	130	177	3- 17-9	000	500.	- 27	857	8/
1 2	5-538 -4	£10*	****	2-31-3	-134	810-	8-45-5	000	.003	2- X-2	107	27.70
<u> </u>	4-733 -4	£10.	. u.3	2-27:-5	-185	910.	9-57 -5	180.	•003	2.84 -3	37.	777.
15	4- 042 -4	610*	£00.	2-13 -3	Tot.	+10-	9.34 -5	1001	£00.	6- 69-2	937-	677-
15	3,453 -4	•10.	700-	2-03 -3	- 18 J	710-	1.03 +	100.	. 003	6- 74-2	60.20	-117
17	2-956 -4	.020	700-	£- 00*7	161.	-010	† 11-1	.00	.003	2-41 -3	117-	-1.14
£	7-275-7	070-	700-	1.34 -3	•133	83.	1.22 4	100-	-002	F- 1F-7	*17.	-1.12
61	5-16J -4	η. 120.	100.	1-53 -3	-195	900-	1-25-1	100	700*	1-99 -3	.216	10
70	1-847 -4	. u 20	100.	1-20 -3	•136	-625	1.9.	100	700-	1.55 -3	-218	97.
7	1-573 -+	. 02v	100.	8-00 -t	161	405	7 % 1	100	700	1-21	-419	107-
77	1-340 -6	170.	100	0.03	961-	571	1.91	700.	700	1 1	(77-	ري. د
53		770-	700	2000	557	700	1 26	700,	700	5- 77-R	177-	
• •	C- 0C/ -	170.	100	2000	A 1	36	200	780	100	10.0	777	
5 7	7.115.55	170	000	10.0	200	3	1007	700		76.0	4563	5 T
	450	720	200	1	007			200			***	
		170	000	1-70	200		1	100		1 1	* 7 7	707
2 5		-021	000	1-31 -4	-200	000	1-07	500	700	4-83 -4	477	100
2		.021	- 000	1-00-1	. 2 00	000	3.03 -5	-003	100	7.67.7	-225	1000
31	3.230 -5	170.	000-	7-68 -5	-200	999	.1.93 -5	.003	300	1-88-1	-225	103-
35	2-815 -5	170-	000	5-88-5	102-	200	9- 78-9	• 003	S	1.55 -4	• 445	.Cu1
£ ;	2-404-5	-021	700-	4-50 -5	107-	200	5-82-5	.003	070	1-27	• 575	101-
4	Z- +CP	170		4.40 -V	107		4.85	3	300	11	577	10.
7	4 C			20.0	100	3			3		22.	
	1-295 -5	170	207	1.55 -5	707	200	3-02	200	3	5-87-5	222	0000
PE	1-115 -5	.021	000	1-19 -5	707	200	2-53-5	. 003	30.	4-63 -5	.225	2001
ě		170.	900-	9-08 -6	107.	000	2-11-5	.003	30.	5- 5-	• 425	000
4.0	8-300 -e	170.	იცი•	9- 96-9	107-	990	L. 865	.003	30.	5- 6F-F	977-	000
41	9- 621.2	120.	con-	5-34 -6	-201	200.	1.52 -5	.003	30.	2-11-5	977.	377
7	6-221 -6	170-	000-	4-38 -6	-201	-000	1-19 -5	.003	300	7-77-7	-226	000
43	5- 198 -6	.021	000	3.13 -5	. 707-	000	9-30-6	.03	30.	1-74 -5	977-	207-
‡	4-692	170*	.000°	5-40 -6	707	000	7-44-5	. dua	200.	1-45 -5	-226	707
÷5	4.084 -6	.021	,00°	1-83 -6	107.	000-	5.76 -6	. 003	30.	1-17 -5	•225	200
Ť,	3-551 -0	170-	000-	1-41 -0	.201	000	4-43 -5	- 603	200-	9-43 -5	-226	000
17	3-106 -5	170.	000.	9- 60-1	707-	000	3.53 -5	.603	30.	7.72 -6	977-	222.
4	2-735 -6	.021	000-	9-78	-201	000-	7- 61-7	- 003	30.	6-35 -6	-226	200
9	5-415	170.	200.	F- 25-9	107	200-	9- 57-7	. 003	30.	2.48 -6	•226	707
50	7-133 -6	-021	000	4.84 -T	- 201	900	1-86 -0	. 003	3	4.4	•256	200

Table 4.17 Parameters at 1.06 microns

						A		5	ِ ا	1	3	F
Ę.	Kaylengh atten.	Caylenge	Cotton	atten.	optical	optical	absorp.	optical	optical	coeff.	optical	optical
	coeff.	thick.	thick.	:: }; ;;	tick S	thick i	coeff.	thick.	thick.		thick.	thick g. f.
(E)	(Fm.')	(g - g)	Î		(n-n)	(m-m)		(n - n)	(m - m)		(n - n)	8 - 5
#	es _n	r _m	` , u	4	r _{er}	ď	6 3	ĵ,	73	Bext	fext	r. ext
9	F.192 -4	ooa.	T.O.	1- 61-1	900.	-179	3	000.	000	1- 91-1	000-	.180
4	1.434 -4	100.	-006	7- 26-4	-031	160°	.	000.	30.	5-40-5	790.	.105
7	4-151-4	100.	cho.	7- 51-7	.111	-062	.	200.	39.	7-17-2	.118	-067
m,	5- 180°5	700-	200	5- 70°6	75].	95.	.	3	30.	9-54 -3	*	100.
4 14	2-140	700	400	01.0	413) i	.	900	3	7.36.43	747	9
٠,	4.922	500	5	61 45	241		.	900		20.7		700
٠,	1 360	500	, tab.	2.35 -3	163	- U30	; 4	000	700	2-15-3	153	660.
	3-516 -4	400	900	74-7	151	976	3	200	30.	4-78 -3	.150	260.
. 0	3.123	500	700	2.36 -3	.159	.025	3	.000	30.	4-6-	.15e	170-
2	2.765 -4	-00	-002	2-27 -5	•156	-023	;	000	200-	5- X:7	191.	•465
11	+- 05+*7	. 005	700-	2-12-3	-158	-021	j	000	mo.	4-37 -3	. 163	770-
71	2.036	, dor	100.	4-62-2	. 160	-018	•	. J.	900-	7.4 -3	• 10¢	070*
	L-733 -4	500.	100-	2.00 -3	-102	ole.	ż	. 65	કુ. જ	₹- \$-7	• 168	270-
71	1-524 -4	300°	100.	5-70-7	•164	•1n•	ಕ	200.	300.	F- 11-7	.170	<10°
: ب	•	900.	100-	£-90 -3	160	-012	.		33	6- 20.2 -3	777	-013
ا ک	1-113 -4	900	Tor.	1-90 -5	. 158	010.	.	000	200	f- 16-1	* T .	440.
-		920	- CO.	1-73 -5	27.	63	.	3	3	1-68 -5	027.	٠ •
a.		900	100.	1.72 -3	7115	200	.	200.	300	7- 26-1	-170	200
2 ;		9	000	L- C1.	• 113	5	.	000	3	1.2	207.	900
2 :	1. 2.5. n	700	999	77.7	71.	\$ 3	.	300	3 6	71	191	
.				7 10 1	77.	555		3	300	7 1	181	500
3 2		700	900	5.65	177	700	: d	900	300	1	183	700-
2		700	000	3-53 -4	177	-00Z	;	GUO.	3	7 5.7	164	-002
ır.		7000	270	+ 16.7	177	130	: .	000	300	7 27 5	\$	100.
\$		700-	900	2.59 -4	.178	13.		200.	200.	7 72.7	184	100.
72		100.	000	1.38 4	-174	.003	.	000.	oco.	2-18 -4	.165	100.
£.		-007	eeo-	+ 7€*1	927-	100-	•	900	300.	1.68	.185	700.
ę,	1.430 -5	Fou.	2000	1-17 -4	.179	, coo	;	. e3c	.	1-31 +	-165	1001
30	1-231 -5	700.	000	6-94-6	P.179	200-	÷.	000	3 00.	7:1	-165	3
.		- Con•	200	6-63	.170	000	; ;	000	3	C- (8.)	- 185	700
¥:	9.055 -6	763.	000	5-53-5	. I.76	300	.	200.	3	() ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	C91-	9
2 7	7 2 3 4	200	900	7 7	27.	000	.		800	7.74	182	200
.	5.663 -6	101	900	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	176	(190)	i d	000	700		145	250
. ≤	4-356-4	200	000	1-50	179	3	5	200	30	¢- 67•7	165	200
**		70n-	000	1-38 -5	621.	000-	•	000	200	1-80 -5	. 185	700-
¥.	3.581 -4	-007	. 200-	1-36 -5	621-	-000	;	oco.	3,.	1.42 -5	.185	222-
65	3.494 -5	-00 7	000.	8.08 -6	.179	000	.	000.	3 00	1-12 -5	. 180	200-
3		70n-	660.	6-19	•119	000-	j	0	999	6-67 -0	997.	2
7		700-	neo.	4.75 -5	.179	2000	ð	000	700	S:	.165	22.
٠,		-607	200.	3-63-10	-179	000	s ·	200.	3	*	C97.	20.
7		~ OO •	300	€- 81.7	×11.	000	.	3	3	۲ ۲	997	7
4		700-	٠ • •	2-13-5	621.	300	.	200.	3	*	9	2
ĵ:	1.315 -5	\car	000	1.65 -5	617-	200	:	200.	3	ר כל י	901.	
9 !		700-	. J.	1-25 -5	-179	200	.	000	3	6- 04-7 6- 04-7	• 18c	20.
	1-001 -6	20.	300	9.50 -7	-179	000	.	000	30.0	9.5	001.	
r c		200-	000	7- 75-7		000	.	200	3	70-1	001.	
2 :	1 0 1 1	200	000	j- 70°C	671.	300	.	3	3 3) i	
ž	1-201	•	>) 10°4	671	3	;	•	3	7- 71-1	001.	•
					,							

Table 4, 18 Parameters at 1,26 microns

Alt.	Rayleagh atten.	Rayleigh optical	Rayleigh optical	Acrosol atten.	Aerosol	Acrosol	Ozone absorp.	Ozone	Ozone	Ext. coeff.	Ext. optical	Ext. optical
(km)	(Fin _1,	(0 - h)	(h - e.)	(Fm ⁻¹	(0 - b)	(h-e)	(km ⁻¹)	(0 - h)	(h-æ)	(Jens ⁻¹)	(0 - p)	(h - ∞)
ď	$eta_{ m r}$	ţ.	T,	β	ď	, d	B3.	73	73	ßext	rext	r ext
ာ	5- 160°7	000-	• 003	1- 30-7	000-	171-	•0	000	900	1-60-1	กกก	.174
~	5.713	000-	£00.	4.75 -2	-078	£60°	.	000	(A)	4.79 -2	820	0 1
~	3-352 -4	100	200°	2- ch-2	7711-	659	.	000	30.5	7- 90-7	£113	700.
4 0 4	2.737	5	700-	6.35 -4	133	1	s a	000	300	4.83	*	3
t r	4- 657		700-	3.4.5 -3	151	*0.	3	700.	300	3.68 -3	461.	. 030
t we	7-507-7	700*	700-	5-74-7	. 140	-031	ં	000	300	2-04-3	-147	.033
٠	1-671 -4	700-	100.	2-52-2	747	670-	÷	- 000	300	2.45 -3	11.	.U3U
o -	1.755 -4	700.	100*	2.32 -3	-154	970*	b	200	200	2.49	141	070.
۲ <u>.</u>	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	700	100	5-77-7	141	770	÷ =	200	3 (3.5)	8.7	1 to 1 to 1	670.
3 -	1.351	• • • • • • • • • • • • • • • • • • • •	100.	2.11.2	161	220-	3 4	200	3	2.15 -3	1	170
: :	7- 7-0-1	600	Too.	2-115	153	840.	; ;	000-	200	2-24 -3	-150	870.
11	6-50% -5	400.	100.	L- 77 -5	451.	-016	3	200.	000	2.Uó -3	-156	olo.
+	7-610 -5	•003	200-	1-33 -3	151.	+10-	3	200.	000-	2.00 -3	091	\$70°
1.5	5-508 -5	.003	200	1-81	661.	710-	3	200-	37	1-86-1	797	710.
۲ ا	5-560 -5	500°	2000	1-72-3	191	070	;	200.	000	1-76 -3	***	30.
,	4.725 -5	509°	000°	5-0-1	797	900	.		000	1.00	991.	V. C.
r 0	4-003	0.0	200	1.15	97.	5	3 3	200	3	1-42	.07	מאריים י
	2 040 C		elet.	200	167	100	j. 4	000	trip's	- G-1	021	*77.
77	€- 575°7	£00°	000.	7.36 -4	.168.	-003	ಕ	770	700	7 3.7	171.	.003
77	5- 551-7	-003	חרף.	5.56 -	- 106	-002	3	7 00 -	300	5.77 -4	727.	-000
5.3	1-837 -5	£(:0-	200.	4-25 -4	691-	700-	;	2000	30.	1 3;	717	700.
77	1.538 -5	£00.	55.	3-37-14	-169	-002	3 :	000	200	7.07		770
<u>;</u> ;	1.337 -5	400.	900	1 1 2 7	-17c	100	.	000	3	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	571.	
	2-785 -5	450	200	1 58-7	170	[25]		200.	300	7 4.1	.173	100.
; 5	3-370 -6	ŧún.	000	1-45-4	170	100-	3	יים מיים	30.	1.55 -4	+11.	100.
€.7	7-173 -0	£0.0.	700-	11-11	.170	200	;	000.	M.	1-13 -4	174	ასეი
3;	9- 0-1-x	200.0	000-	8 - 14 - 15 - 15 - 15 - 15 - 15 - 15 - 15	-170	925	;	2000	3	5-14-6	*I.	300
7:	2.44	600	3		171	3	.	000	30	5,45	174	200
7 5	- 126. - 1-15.	£00.	967.	3-33 -5	111.	500		.65.	300	4.41 -5	114	000
		£00.	000	<- 5ۥZ	.171	oon-	;	2	30.	5-67-6	*17*	999
	* 4.647 -5	•003	. u.a.	2-52-2	171	300	.	300.	30°	2-55-2	727	3000
<u>.</u>	Z-424-A	£00.	000	5 7.1	7.1.	9	.	2 3	3	C 05.	72.	000
.	C= 760-7	400°	000	C 76-1	7.1.	200	\$ 5	100	3	C- 61-1	***	700
r u	1.545	1000	207	4 77-1	111	000	3	3 000	000	9-17-6	*11.	,000
• ;	, , , , , , , , , , , , , , , , , , ,	500	,,,,	5-36-5	171.	000	;	700	CCO.	7.45 -0	174	300
7-	1-154 -5	ton.	900	4.54 -3	.171	0.0	ď	eno.	(201)	2.59 -6	-174	Opp.
74	_	£0.7=	0 000	3-17 -6	171.	-000	ទំ ។	3000	25.	C- 24°4	21	700.
(33	1 7 7 9 9 0	£00.		0- 9c•7	111.	200	.	700	37	4.55 -5	ži:	200
4 !	495.4	, , , ,	2	C- +5.7	7/1-		.	000	3	0- 63-7		2
	5.55° -7	500	000	6.50	171	200	3 5	200	30	6 F 22 - 5	***	200
- - - - -	4.303 -7	400.	000	7- 11- A	1771	200	0	900.	30.	10.46 -0	174	
4	7- 6-5-7	2000	000.	7-00-7	1210	200	3	2000	30.	1-14 -5	.174	200
Ç,	5- 45E.k	£00.	ner.	5-37 -7	171.	200.	 •	. 000	.	1- 97-6	174	200.
n G	3.430 -7	c 03.	Orr-	4-i1 -7	171.	200	;	200.		マネン	.174	200

Table 4,19 Parameters at 1,67 microns

coeff. (k:a) (km ⁻¹) h β_{Γ}	7		451711		- Line	dicaria.	-				
	thick. (0 - h)	, thick. (h - 8)	coeff. (km ⁻¹)	thick. (0 - h)	thick. (h-∞)	coeff. (km ⁻¹)	thick. (0 - h)	thick. (h - ss)	(km ⁻¹)	(0 - h)	mick. (h - ∞)
	۴.	. .	β	r _e	٠,۵	β3	r _S	13	ext	rx txx	T ext
1- 325 -4	600.	.301	5- 0°5	.00.	.155	ŝ	000.	٥٠٥٠	9-81 -¢	ייטני.	101.
t- fol-1	200	400-	7- 16-7	720-	400.	.	6 000.	.00.	7- 76-4	170-	0) (0) (0) (
1. uRu))	100.	1.35 -2	101.	400.	.	000	7	7- 16-2	115	1177
		1000	(- 1 4 - 3 (- 1 4 - 3		440	; o	300	230	4.22 -3	.121	-035
	100	100.	3.11 - 1	+71•	150.	3	000	200.	5- 67-5	-175	460.
7-1-2	100.	100.	2-20 -5	1715	• 028	3	200	.	6-17-7	177	477.
595.0	100°	25C.	6- 40-2	671.	970.	;	7 CO .	1 00.	6- 01-7	061	070.
	loo.	2000	2-10 -3	151.	470°	.	300°	77	2- 61-7	1.132	+70.
	100	200	2 - 75 · ·	61.	770-	3 3	200	22	2-40-2	1.4	070.
		200	1.46 -3	701	910	3	000	33.	60-1	.138	040.
		77	1-34-5	133	910.	3	000.	500.	1.37 -5	.140	010.
	100	, 100	1- 62-1	191.	\$10°	3	200.	• 000	1-85 -3	751-	+ 10.
2.439	100.	222.	1.75 -5	.143	-10.	. .	ຕາດດ	30-	1.77 5	.143	
if 2-101-5	100.	566.	L- 9c-1	.144	110.	j	• • • • • • • • • • • • • • • • • • •	700	£- 50.1		110
1.730	100.	200.	1.55 -5	-140	¥00.	.) .	2	6- 66-7	147	
1.515	100-	: :	1.074 -5	141	200	.	999	5	C - 20' -	1 5	9 6
	100.	000	1.44 -3 -44 -4		3000	.		777	1.27 -3	151.	
771-1	500	9 :	9- 4/-6	10.1	401.	3 3	200.	000	7- 3-5	.154	400.
		300	9- DZ-c	761.	£05	3	oco.	000-	6.73 -4	.153	400.
4.051	100	000	5-04-14	.153	700-	;	טייי.	2 00.	5-11 -4	.154	, UU.
23 5-935	100.	opo-	3-30 -6	151	700-	ન	, uou	6.0.	3.34 -4	\$C7.	700-
5.034	100-	000-	3-05-1	+67.	100.	.	200	2 2	11.0	151	100.
	100.	000°	4- JC*7	÷C7•	100	• •	000		\$- 87°7	135	100
	1000	200	7- 72-1	156		3	06.00		+ 2:	125	100.
7.735	100	227	1-31 -4	154	מחח.	3	222	200.	1- 15-1	.155	100.
2.317	100.	200.	1-01	•155	000.	•	250.	٠,	1-03-4	- 156	200.
	106.	900.	7-75 -5	.152	.000°	÷	000°	700	c- ch-1	c41.))
1.734	100.	ncr.	5-34-5	5:10	35.	.	000)))	C- 60.3	961.	000
1.453	100.	000	4.04	155	200	• ÷	200	3	200	156	2
	100	200	0	155		; ;	2 2	200	2-77-5	.150	2
7.1.1	100	30.5	2. 36 - 2	•155	220	÷	200		c- f1-7	.152	200
7.831	100.	200	1.56 -5	155	000	÷	000.	າ ດຸດ	5- 45-1	.150	.000
£.768	100.	nor.	1.20 -5	.155	000-	;	000.	لىن.	1.20 -5	. 150	200
5.790	100.	000.	5.13 ->	•155	200-	້	200.	700	•	4.20) ·
766*5	100.	000	7.01 -5	155	000	;	D	יים י	3-16-1	007.	0 1
116.7	100	000	5-36-5	• L55	200	\$ 1	200	3	0.04.4	1 4	200
1- 671-6	100	200	4-15-5	551.	000		200	200	3-47 -t	150	
40.81	i de G	200	2-41 -5	.155	ם מיני	3	Juo.	30.	c- 69°7	.150	200
2.437	100	000.	1.35.	.155	, O.C.	÷	222.	200	5- 50-7	.15	2 2 1
	106.	200	c- 14°7	.155	200.	•	. O.O.	٠٠٠	1.55 -t	•150	200
F+9+1	400.	J. J.	1-09 -	•155	3200	3	2	20.	1-27	. 150	200
1-615	1000	000-	8.31 -7	•155	າດດ-	.	, 000.		7- 56-6	401	0 :
	100	25.	5.33 -7	\$c]•	000	• ·	200	3	10.1		000
1- 467-4	100.	960.	1- 500 m	-100 	200	.	000	3 0		9.4	

Table 4.20 Parameters at 2.17 microns

Alt.	Rayleigh	Rayleigh	Rayleigh	Aerosol	Aerosol	Acrosol	Ozome	Grone	1	13		
	atten.	optical	optical	atten.	optical	optical	ahsom	ontical	Oction	EXI.	EXI.	Ext.
(L a)	COCET.	thick.	thick	coeff.	thick.	thick.	coeff.	thick.	thick.		opucai	opuca thick
) (1)		(u - u)	8 ·	(Km ⁻¹)	(Q - P)	(µ-∞)	(km ⁻¹)	(0 - h)	(h - 8)	(km ⁻¹)	(0 - h)	(h - 8)
-	20°	<u>.</u>	, L	8g d	*	, <u>r</u> a	B ₃	73	E	β _{ext}	rext	ext
2	6-624-5	000-	2000	3- uc-8	000.	451.	, 5	upp.	tale.	7	I dive	
	£-200-5	.00°	000-	3.74 -2	100.	-073	; ;	222	200	7 72 4	1 1 1	7.
~ ~	3-603-6	77.7	٠,٠,٠	7- 15-1	.083	• 146	• •	000.	200	1-04-4	1000	740
n 4	3.430 -3	200	200	6.78 -3	かいつ・	-035	.	200.	200.	6-81-3	100	2
1 11		3	200	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<u>-</u>	050-	·3	7000	3	3.51 -3	c 01.	365
٠.,	2-182-2	000		2-70-3	- L.C.	-027	.	. 000	770	4-73 -3	-103	1750
. •		3 2		1.40 -5	31.	570-	.	220.	eso.	1-93 -3	.113	270.
tr.	1-237 -5	200	2000	1.47 -5	777	770-	.	00.	000-	1.79 -5	711-	470.
· (P	1.765 -5	200	200	1.75 -3	\$77 .	170.	.	200	200	1-84-5	• 114	170.
3	1.562 -5	200	2000	1-11	111.	210	i d	900	3 3	2 - 2 - 7	311	\$ P
17	1.570 -5	• 000	Cot.	f- pc-7	677.	910-	; ;	9 2	200	27.7	111.	
71	1-173>	000	000.	1.73 -3	.120	410.		000	200	7 79 7	677	
]	1.037 -2	500.	000-	1.55 -3	771.	210.	3	200	200	, i	777	
4 .	c- 609*2	٠ د د د د	DO:	1.52 -3	+71.	110.	3	200.	300.	1.53 -	144	1 7 7
57	7-555	က (၁)	מחר.	1.63 -3	-175	600°	3	200.	250.	1-43 -3	-145	****
. 1	5 477	200	מחוף.	1.35 -5	-170	20.	÷	.00°		1-30 -3	177.	000
. 7	C 100 7		000	1-34-3	671.	- 00 ·	•	333.	300-	1.4-34	•126	F00.
	31 37 37	200	900	1. 30 -5	671-	500.	້	, U.S.	300.	1-30 -5	. 150	()7.
. 07		200	900	1-0-4); ;	***	.	٠ •	300	1-10 -3	161.	*20.
7.	•	200	000	20.00	761	500	.	000	000	4- 60.	-132	£ 10.
77	2-433 -5	200.	000	4-37 -4	137	700	3 3		300	\$1 +0 · 0	261.	700.
72	2-073 -6	000-	.000	3.35 -4	661.	100-	; ;	200	3	1 1 1		700
7. 7	1.774 -	000.	2000	7- 54.7	-133	100	3 3	200	300	1 17	. 133	,
5.5	4- 515-7	20.3.		4- 67-7	.133	1001	3	200	3	4. 52.2	*	7.7
52	2- 767-1	٠٠ ٠ ٠	000.	1.35 -4	•134	100.	.	uCi.	30.	4- 06-1	134	
, ,	101-1 101-1	יייי פריייייייייייייייייייייייייייייייי	JC0 .	7- 65-1	-134	100-	3	000.	200.	1-50 -4	134	100
5 2	7-11-1	000	ייייי	\$- 10 C	41.16	າຕາ	•	000.	(J.)	4- 51 -+	+61.	300.
, .3	6-956 -1	200	000	2017	•134	000	.	77	200.	6-d5-6	-134	300.
1		3	200	5-14-5		2.5	.	000.	3	C- 12-3	-135	??
3.2	2-177-5	600.	000.	3- 56-6	76.1.	900	: 4	200	3	C- 07-7	C6.1.	2
£ 4.	4-575 -7	ייים"	יייי.	3.01 -5	451.	200	3	777	200		1.45	200
4 '	3-750 -7	000		5- 16-7	+114	0.00	3	200.	300	Z- 55.5	200	
	7- 667-6)) (000	1.77 -5	\$£7.	000	÷	000	200.	1-30 -5	.135	200
<u>.</u>	7- 354-3	000		1. 30 -1 0 - 1	\$ T .	200	ď.	3001	. 000	1-33 -5	3.1.5	000
1	2-670-2			7 70 7	*:	3	.) ()	707.	1.06 -5	. 135	000.
¥	1-744 -7	000	222	2000	35		3 4	200	20.5	8-15-5	. 1.35	.
.;	1-510 -7	000 -	996	4.5c -u	-134	2000	3 5	200	200	9- 6-4	67.	3 :
7	1.305 -7	, U U U	000-	3-57 -5	- 134 ·	2000	•	000.	777	2. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	36	7 7
7+	1-152 -7	700	300	2-13 -5	•134	000-	4	220.	2000	2.85 -6	5010	200
1 4		6 G	200	70.7	• 134 ·	000	• •	000.	000	4-13 -v	£1.15	200
Ţ		200		1.14	• 1 34 • 1 34	000	ร้ :	300	35.	4-60-1	5115	000.
. (1		1000	e e	2 4 4 G	171	3	•	200	3	٥- ١٠٠١	54.	200.
· K+	5-6-6-3	200	200	7-71	75 1 .	3	.	000	25.	7- 70-7	CC 1 •	200.
u.	** ST -3	200	200	5-54 -7		200	. <i>j</i>	000	3		C\$ 1.	00°
04		70.01	000	4.23 -7	134	223	,	200	9 2	5.4	٠٠ . اور	2.5
J.	3.933 -6	000.	000-	1- 77-5	134		÷	200	CAG.	4.64 -7	54.1	7
)))) } •		:	2

Table 4.21 Parameters at 3.50 microns

。 《中国社会》是一种特别的一种,是一种特别的一种,是一种的一种的一种的一种的一种的一种的一种,是一种的一种的一种的一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,是一种的社会,也是一种的社会,是一种的社会,是一种的社会,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是一种的一种,也是

		atten.	Kzykenen atten.	optical	optical	Actual atten.	optical	optical	Ozone absorp.	Optical	Ozone	ext. coeff.	ext.	Ext. opti:al
	T. T	<u>\$</u>	±€.	(0 - h)	(h - 8)	(Em. ²).	(0 - b)	(k - 8)	(FB -1)	(9 - h)	thick.	(km ⁻¹)	thick. (0 - b)	्र इ.स.
	111. 101. 101. 2-0.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0.	6 2.	.	, L	, , ,	g D	T.	, d	ß ₃	ř.	73	fext	rext	r. et
1111	1.000	8.4	23 -3	0000	0000	7- 00-1	700.	1111	2	0 00.	(MÖ.	7- 80-1	200.	177
	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	7	ر انتار	200	000-	3-08	uçn.	-000	3	000	.00	3.08 -2	. USO.	100
	1,	ים יים יים	•	ر ال	250.	1.53 -6	710-	86.00	ခံရ	000	3	1-33 -2	270-	961
1111 1	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	. 4		200	222	00°0 00°0 00°0 00°0	250.	925		200	33			77.
	1000	;		973	270	7-77-7	560.	770-		000	000-	4-43-5	580*	27.10
	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	3.0	•	0000	JC0.	4-57 -3	150·	070-	;	200-	30.	1.57 -3	16a.	
	1000 0000 1117 2-1 1100 0000 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 0000 1100 0000 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 1100 0000 11	3-6		ر د د د	300.	1.60 -5	750.	670		000	3	7 7	760.	-1.17
		7		200	3.	1-30-5	460	110-		000	7	7 7	\$5.0°	:
111					377	1-60-1	1.50	410-	3 3	200.	30.5	14-1	LEO.	
1000		7-0		000	2000	1.32 -5	. u96	.013	÷	.000	300	1-32 -3	840.	
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		1.7		200	070.	1-30 -3	540.	110-	;	. 000	• 200	1-36 -5	650.	* * * *
1,		1.4		200	000-	1-20 -5	101.	370-	.	. U.S.	20.	1.28 -3	101.	27.
111		7•1		ביים י	, J.C.	1-25 -3	701.	600	.	200	3	6- 07-1	701	70.
100		7		200	200	77.77	507	000		200		() () () () () () () () () ()	40.1	97
1,		7.0		3	900	1-10-5	501	500	id	200	300	1-10 -5	501	1
1000	-7 .000 .000			3	000	1-07	100	\$50°	5	000	30.0	1-07	901.	+ > -
11	-7 .000 .000 .2.75 -4 .103 .002 .002 .002 .003 .000 .000 .000 .0	7.0		cen.	0000	4- 56 -8	101	£00°	.	000	30.	4- 00·c	-107	£0.1-
100	-7 .000 .000 .276 -4 .103 .002 .002 .003 .003 .000 .000 .000 .0	4.0		eno.	ວຽດ.	6.3J -4	103	£500.	;	. 040	900	5-61 -4	. 103	507.
111	- 1	7-7		100.	000.	4-73 -4	.103	700-	.		ر الاراب	4-17-4	.104	700-
	- 1000	40 S		000		3-20	507	770	.	3	3	3-37	501.	7000
	-7	2.6		200	000	#= SI*7	, 104 104	100	• ÷	200	3	\$- E1-7	677	7
111	-7			200	000	3- 35-1	217	100	l s	מויני.	300	1-84-4	011.	100
		1.0		200	000.	1.50 -4	110	100.	3 3	.050	300	1-01	.11.	100.
-7 - 0000	-7 .000 .000	1.6		600.	2000	1-23 -4	.110	000-	.	.000	.	1-67-1	011-	do:).
	-7		2- B5	200.	ero.	4-35 -5	.110	999	j	200.	70.0	C- 74.5	011-	300.
- 1	-7 -000 -000 -000 -5.24 -5 -110 -000 -08 -000 -000 -0.00 -5.24 -5 -111 -000 -09 -000 -0.00 -1.40 -5 -111 -000 -09 -000 -0.00 -1.40 -5 -111 -000 -09 -000 -0.00 -1.40 -5 -111 -000 -09 -000 -0.00 -0.00 -5.55 -5 -111 -000 -09 -000 -0.00 -0.00 -5.55 -5 -111 -000 -09 -000 -0.00 -0.00 -5.55 -5 -111 -000 -09 -000 -0.00 -0.00 -5.55 -5 -111 -0.00 -09 -000 -0.00 -0.00 -0.00 -0.00 -09 -000 -0.00 -0.00 -0.00 -0.00 -09 -000 -0.	7-7		, c	•00.	2-77-1	.110	000	.	. Juli	ري. د	7-43 -5	011-	2021
		7) () ()	000	5-14-15 4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	011.	900	3 :	100	200		111	3
				900	999	2.47.4	21.	900	3 2	CPP T	(T) 0	3.25 -5	777-	300
		,		300	,	5- 84-7	111.	000	3		3	7- 64-7	1111	200
		5.5			300	i-90 -5	111	onn•	· •	060	300	1.31 -5	111.	aŭ.
-3 .000 .000 .000 .000 .000 .000 .000 .0	-3 .000 .000 8.55 -5 .111 .000 03 .000 .000 8.55 -5 .111 .000 03 .000 .000 8.55 -5 .111 .000 03 .000 .000 8.45 -5 .111 .000 03 .000 .000 8.45 -5 .111 .000 03 .000 .000 8.45 -5 .111 .000 03 .000 .000 8.45 -5 .111 .000 04 .000 .000 8.45 -5 .111 .000 05 .000 .000 8.45 -7 .111 .000 06 .000 .000 8.45 -7 .111 .000 07 .000 .000 8.45 -7 .111 .000 07 .000 .000 8.45 -7 .111 .000 07 .000 .000 8.45 -7 .111 .000 07 .000 .000 8.45 -7 .111 .000 0.	4.7		000.	3000	1-60	1111	ם פריי	່ວ່	200	ر ا ا	S- 04-	111-	700.
-3 .000 .000 .000 .000 .000 .000 .000 .0		4 8		50.0	700.	C- 71.1	171	200	.	300	300	C- 71.1	1774	200
-9 .000 .000 .000 .000 .000 .000 .000 .0	-8 .000 .000 .000 .000 .000 .000 .000 .0			900	200	46.64	111	ore:	.	000	800	4	177-	2
-4 .000 .000 .000 .000 .000 .000 .000 .0	-3 .000 .000 2.34 -6 .111 .000 03 .000 .000 2.25 -5 .111 .000 03 .000 .000 1.22 -5 .111 .000 03 .000 .000 1.32 -6 .111 .000 04 .000 .000 1.32 -5 .111 .000 05 .000 .000 1.35 -7 .111 .000 06 .000 .000 2.35 -7 .111 .000 07 .000 .000 2.55 -7 .111 .000 08 .000 .000 2.57 -7 .111 .000 0.	7.5		200	מירי.	5-01-5	111	900	3	000	3	d- 25.0	111-	730
-3 .000 .000 2.25 -0 .111 .000 0000 .000 2.27 -5 .111 .000 0000 .000 .000 .000 .000	-3 .000 .000 2.25 -0 .111 .000 03 .000 .000 1.72 -0 .111 .000 03 .000 .000 1.72 -5 .111 .000 04 .000 .000 1.52 -5 .111 .000 05 .000 .000 1.51 -7 .111 .000 07 .000 .000 2.35 -7 .111 .000 07 .000 .000 2.35 -7 .111 .000 07 .000 .000 2.55 -7 .111 .000 07 .000 .000 2.57 -7 .111 .000 0.	7•7		.000	JUC.	3-34 -6	1111	GWG.	· •	.000	30.	3-46 -6	111.	200.
-3 .000 .000 .000 1.72 -5 .111 .000 0000 .000 1.77 -5 .111 .000 0000 .000 1.77 -5 .111 .000 0000 1.77 -5 .111 .000 0000 1.75 -5 .111 .000 0000 1.35 -7 .111 .000 0000 1.000 1.35 -7 .111 .000 0000 1.000 1.35 -7 .111 .000 0000 1.000 1.35 -7 .111 .000 0000 1.000 1.35 -7 .111 .000 0000 1.000	-3 .000 .000 1.72 -6 .111 .000 02 .000 .000 1.72 -6 .111 .000 03 .000 .000 1.31 -6 .111 .000 04 .000 .000 1.31 -5 .111 .000 05 .000 .000 5.94 -7 .111 .000 07 .000 .000 5.94 -7 .111 .000 08 .000 .000 5.94 -7 .111 .000 09 .000 .000 5.94 -7 .111 .000 01 .000 .000 5.94 -7 .111 .000 0.	1.3		-000	200.	6- 34-7	111-	00r•	•	000	2000	9- 06-7	777-	200
-2 .000 .000 1.72 -5 .111 .000 0000 1.77 -5 .111 .000 0000 1.77 -5 .111 .000 0000 1.00 1.41 -5 .411 .000 0000 1.00 1.01 -5 .411 .000 0000 1.00 1.01 -5 .411 .000 0000 1.00	-3 .000 .000	¥•1		000		2-52-7	111	٥٦٥.	•	700.	۵,	5- 17-7	1110	3000
-3 .000 .000 1.52 -5 .111 .000 0000 .000 1.53 -0 .111 .000 .000 .000 .000 1.53 -0 .111 .000 .000 1.53 -0 .111 .000 .000 1.53 -7 .111 .000 .000 .000 1.53 -7 .111 .000 .000 .000 .000 .000 .000 .00	-3	i • 4		COO.	200.	1.72 -5	111	000	.		3	1.7.	111-	300.
		7-1		200	200	1.32 -5	11.	200	ວ່	000.		1.35	1 1 1	2011
-1		• •		3	000	C- 10.7	717-	3	.	9	3	7 90 7		
		, ,	7.	000	05.5	1-51-1	#	200	.	200	9	1.35	141.	
					3	1 11 11	117.	00.	;	100	3 3	7- 4- 4	1 1 1	
111. T- 27.5 000. 000. 000. 114. T- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7-		7.	֓֞֝֟֝֜֝֟֝֟֝֟֝֟֝֟֝֝֟֝֟֝֟֝֟֝֟֝֟֝֟ ֪֪֓֓֓֓֞֓֞֞	707		7- 64-4			.	(1117)	300	7- 55-4	111	7000
		5.7		1000	000	1.37 -7		000		000	CO.	1- 71-7	111.	350.

S. S. Sp. Spolena

a gran was the

Table 4.22 Parameters at 4.09 microns

# 3	1	Acrosoi
(m) (m) (m) (m) (m) (m) (m) (m)	F_3 T_3 T_3 F_{ext} T_{ext} T_{ext	thick
### ### ### ### ### ### ### ### ### ##	1	(n-0)
4	0011 600 7.7 7.7 7.7 900 <td>T.</td>	T.
	\$\frac{1}{2}\$\frac	
	200 - 000 -	•
	1000	•
######################################	1000	020° +10° C-
######################################	0.000	
4	100. 1.1	810- 280- 1-
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1000	•
######################################	200	•
2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.000 0.000 1.15 -5 -1 0.001 0.000 0	• ogo • •
######################################	0.000	•
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1.10	,
1	0	- 5-0- 6-
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.000. 0.000	•
4	10.0	•
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1000	1. 1994 .
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